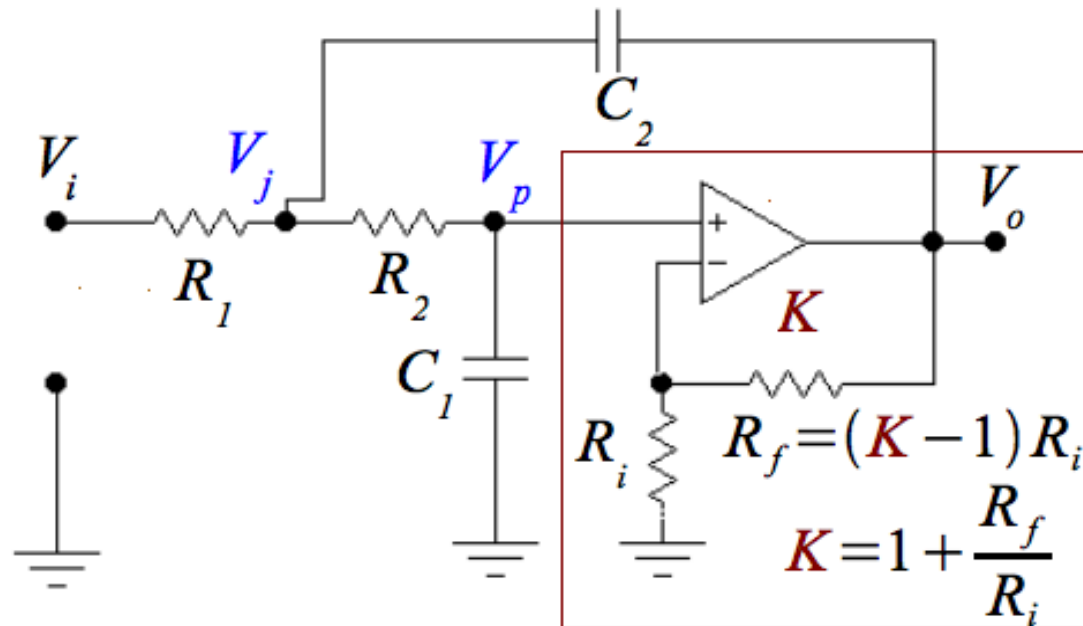




## Single-Amplifier-Biquad (SAB) Filter Stages

- **Sallen and Key Lowpass (LP) Stage**
  - $R_1C_1 = R_2C_2 = RC$  strategy
  - $R_1C_1 \neq R_2C_2$  strategy
- **Sallen and Key Highpass (HP) Stage**
  - LP to HP Transformation
- **Delyannis-Friend Bandpass (BP) Stage**
-

## Sallen-Key LP Stage



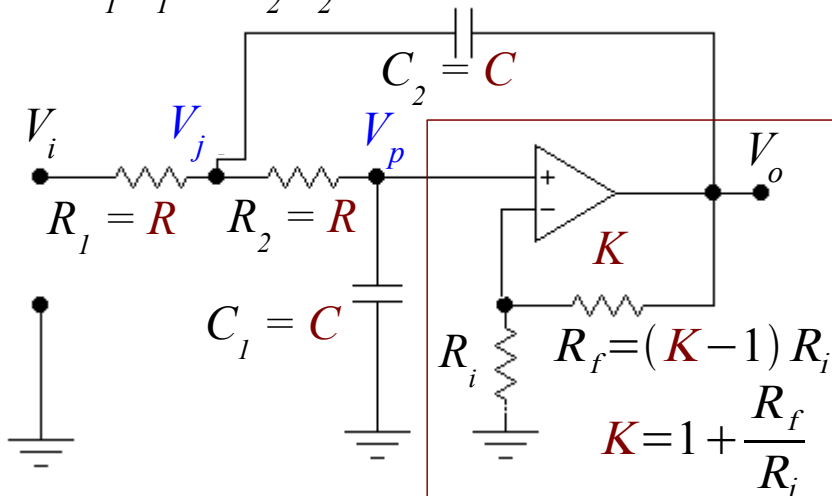
$$G(s) = \frac{V_o}{V_i} = \frac{\omega_0^2 K_0}{s^2 + \frac{\omega_0}{Q} s + \omega_0^2}$$

Choice of **dependent element variables** is important!

1. Choose  $R_1 C_1 = R_2 C_2 = RC \Rightarrow RC \rightarrow 1/\omega_0$  &  $K \rightarrow 1/Q, K_0$
2. Choose  $K$ , say  $K = 1 \Rightarrow K_0 = 1, R_1, R_2, C_1, C_2 \rightarrow 1/\omega_0, 1/Q$

## Sallen-Key LP Stage Analysis

LET  $R_1 C_1 = R_2 C_2 = RC$



Multiplying by  $R$ :

$$V_j: V_j + sCR(V_j - V_o) + V_j - V_p = V_i$$

$$V_p: V_p - V_j + sCRV_p = 0$$

and  $V_o = KV_p$

Eliminate  $V_p$  using  $V_o = KV_p$ ,

and combine terms:

$$V_j: (2 + sCR)V_j - \left(\frac{1}{K} + sCR\right)V_o = V_i$$

$$V_o: -V_j + (1 + sCR)\frac{V_o}{K} = 0$$

Write 2 node equations:

$$V_j: \frac{V_j - V_i}{R} + sC(V_j - V_o) + \frac{V_j - V_p}{R} = 0$$

$$V_p: \frac{V_p - V_j}{R} + sCV_p = 0$$

and  $V_o = KV_p$

## Sallen-Key LP Stage Analysis - cont.

$$V_j: (2 + sCR) V_j - \left(\frac{1}{K} + sCR\right) V_o = V_i$$

$$V_o: -V_j + (1 + sCR) \frac{V_o}{K} = 0$$

Eliminate:  $V_j$  (multiply  $V_o$  Eq by  $(2 + sCR)$ )

$$V_j: (2 + sCR) V_j - \left(\frac{1}{K} + sCR\right) V_o = V_i$$

$$V_o: -(2 + sCR) V_j + (2 + sCR)(1 + sCR) \frac{V_o}{K} = 0$$

Add and solve for  $V_o$  and multiply by  $K$ :

$$\left[ \frac{1}{K} (2 + sCR)(1 + sCR) - \left(\frac{1}{K} + sCR\right) \right] V_o = V_i$$

$$\left[ (2 + sCR)(1 + sCR) - (1 + sKCR) \right] V_o = K V_i$$

## Sallen-Key LP Stage Analysis - cont.

$$\left[ (2 + sCR)(1 + sCR) - (1 + sKCR) \right] V_o = K V_i$$

Multiplying to expand into a polynomial:

$$\left[ (sCR)^2 + 3sCR + 2 - 1 - sKCR \right] V_o = K V_i$$

Collecting terms:

$$\left[ s^2 (CR)^2 + (3 - K) sCR + 1 \right] V_o = K V_i$$

Dividing by  $(CR)^2$ :

$$\left[ s^2 + \frac{(3 - K)}{CR} s + \left( \frac{1}{CR} \right)^2 \right] V_o = K \left( \frac{1}{CR} \right)^2 V_i$$



## Sallen-Key LP Stage Analysis - cont.

$$\left[ s^2 + \frac{(3-K)}{CR} s + \left( \frac{1}{CR} \right)^2 \right] V_o = K \left( \frac{1}{CR} \right)^2 V_i \quad \text{For } R_1 C_1 = R_2 C_2 = RC$$

Form  $G(s) = V_o/V_i$ :

$$G(s) = \frac{V_o}{V_i} = \frac{\left( \frac{1}{CR} \right)^2 K}{s^2 + \frac{(3-K)}{CR} s + \left( \frac{1}{CR} \right)^2} = \frac{\omega_0^2 K_0}{s^2 + \frac{\omega_0}{Q} s + \omega_0^2}$$

$$\omega_0 = \frac{1}{CR} \quad Q = \frac{1}{3-K}$$

Note:  $K=1 \Rightarrow Q = \frac{1}{2}$

sensitivity & potential stability problem, i.e.  $K \geq 3 \Rightarrow G(s)$  unstable



## Sallen-Key LP Stage Analysis - cont.

Design Equations:

$$G(s) = \frac{V_o}{V_i} = \frac{\left(\frac{1}{CR}\right)^2 K}{s^2 + \frac{(3-K)}{CR} s + \left(\frac{1}{CR}\right)^2} = \frac{\omega_0^2 K_0}{s^2 + \frac{\omega_0}{Q} s + \omega_0^2}$$

$$\omega_0 = \frac{1}{CR} : \text{choose } C \Rightarrow R = \frac{1}{C\omega_0}$$

$$Q = \frac{1}{3-K} : \Rightarrow K = 3 - \frac{1}{Q} \quad \begin{array}{l} Q \geq 1/2 \text{ to be realizable, i.e. } K \geq 1 \\ Q \geq 1/2 \text{ to be realizable, i.e. } R_f \geq 0 \end{array}$$

$$K = 1 + \frac{R_f}{R_i} : \text{choose } R_i \Rightarrow R_f = R_i \left(2 - \frac{1}{Q}\right)$$



## Sallen-Key 20 kHz MFM LP Stage

1. Let's do the initial design with normalized  $R$  and  $C$ .

$$\Omega_0 = \omega_0 = \frac{1}{CR} = 2\pi \cdot 20 \cdot 10^3 \quad \text{and} \quad R_0 = 1 \text{ k}\Omega$$

$$G(s_n) = \frac{K / (R_n C_n)^2}{s_n^2 + \frac{(3-K)}{R_n C_n} s_n + \frac{1}{(R_n C_n)^2}} = \frac{K_0}{s_n^2 + \frac{1}{Q} s_n + 1} = \frac{K_0}{s_n^2 + \sqrt{2} s_n + 1}$$

$Q = \frac{1}{\sqrt{2}}$

Normalized design equations:

$$\frac{1}{R_n C_n} = 1 \quad \text{and} \quad K = 1 + \frac{R_{fn}}{R_{in}} = 3 - \frac{1}{Q} = 3 - \sqrt{2} = 1.586$$

where  $R_n = \frac{R}{R_0}$  and  $C_n = \Omega_0 R_0 C$

Choose:  $C_n = 1 \Rightarrow R_n = 1$

Choose:  $R_{in} = 10 \Rightarrow R_{fn} = 5.86$



## *Sallen-Key 20 kHz MFM LP Stage - cont.*

$$C_n = 1 \Rightarrow R_n = 1 \quad \text{where } \Omega_0 = \omega_0 = 2\pi \cdot 20 \cdot 10^3 \quad \text{and} \quad R_0 = 1 \text{ k}\Omega$$

$$C = \frac{C_n}{\Omega_0 R_0} F = \frac{1}{2\pi \cdot 20 \cdot 10^3} \frac{1}{R_0} F = \frac{25}{\pi} \frac{1}{R_0} \mu F = \frac{7.96}{R_0} \mu F$$

$$R = R_n R_0 \Omega$$

$$R_0 = 1 \text{ k}\Omega \Rightarrow \boxed{R = 1 \text{ k}\Omega \quad \text{and} \quad C = 7.96 \text{ nF}}$$

$$R_{in} = 10 \Rightarrow R_{fn} = 5.86$$

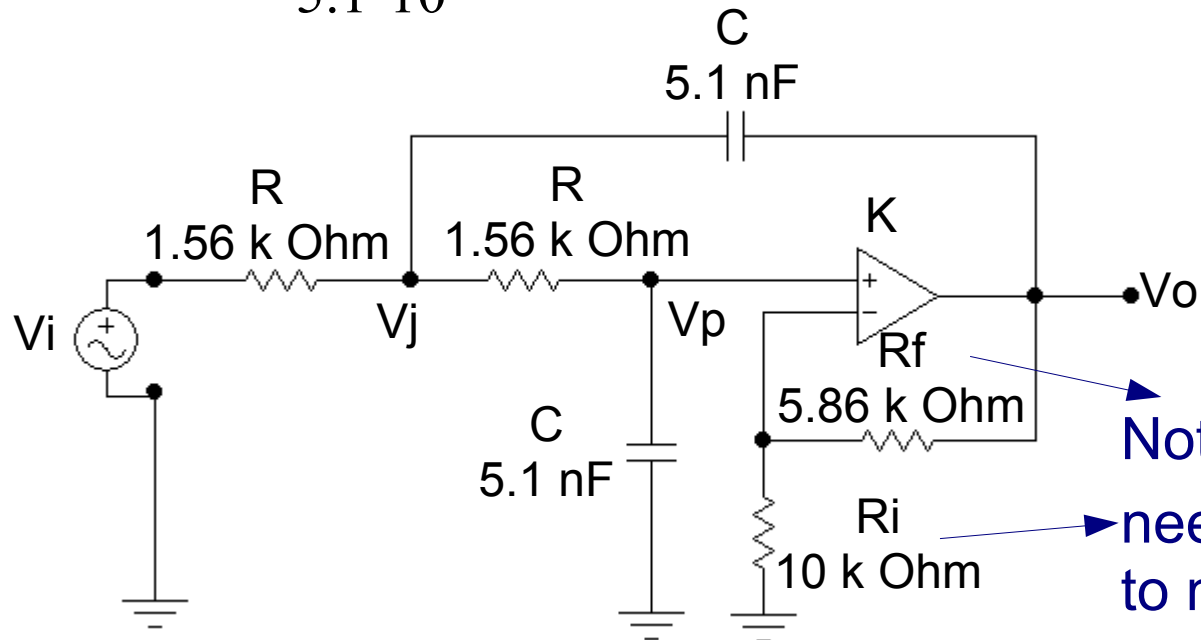
$$R_0 = 1 \text{ k}\Omega \Rightarrow \boxed{R_i = 10 \text{ k}\Omega \quad \text{and} \quad R_f = 5.86 \text{ k}\Omega}$$

## *Sallen-Key 20 kHz MFM LP Stage - cont.*

Suppose we wanted to choose  $C = 5.1 \text{ nF}$  from the RCA Lab.

$$5.1 \text{ nF} = \frac{7.96}{R_0} \mu\text{F} \Rightarrow 5.1 \cdot 10^{-9} = \frac{7.96 \cdot 10^{-6}}{R_0}$$

Solving for  $R_0$ :  $R_0 = \frac{7.96 \cdot 10^{-6}}{5.1 \cdot 10^{-9}} = 1.56 \text{ k}\Omega \Rightarrow \boxed{R = 1.56 \text{ k}\Omega}$

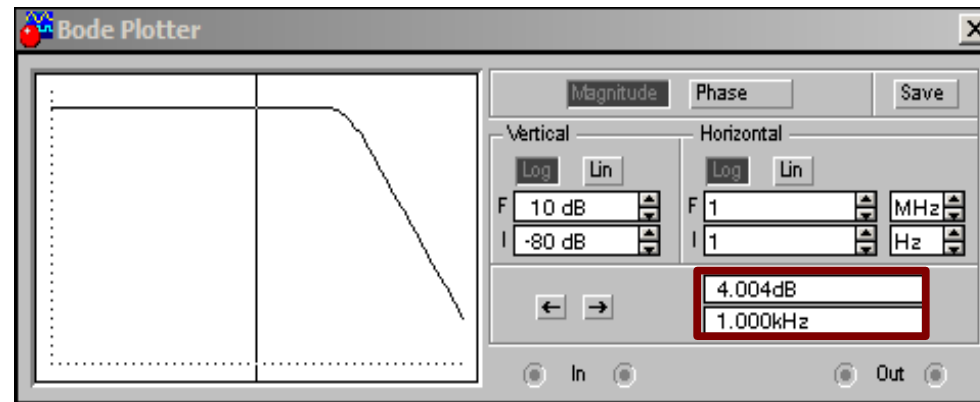


Note:  $R_f$  &  $R_i$  do not need to be rescaled to new  $R_0$ .

## Simulation Results

$$K = 1.586 \Rightarrow 20 \log_{10} |T(j0)| = 20 \log_{10} K = 4 \text{ dB}$$

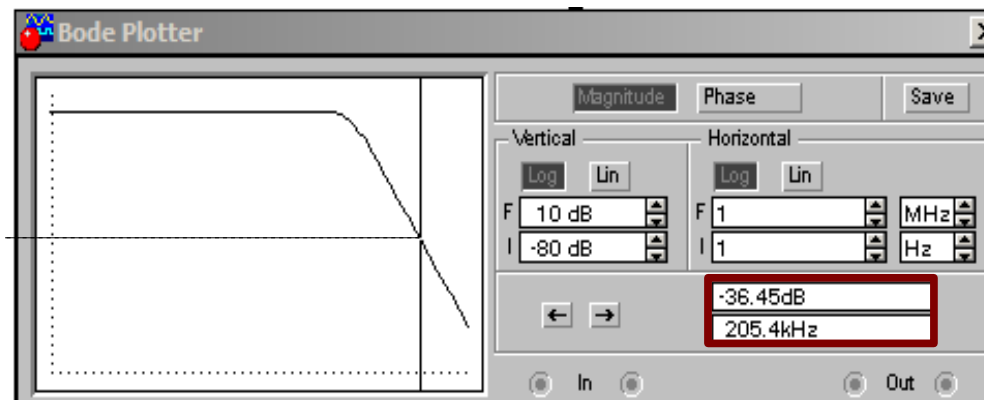
4 dB  
Pass-band Gain



1 kHz

Stop-band Gain  
at 10x cutoff (20 kHz)

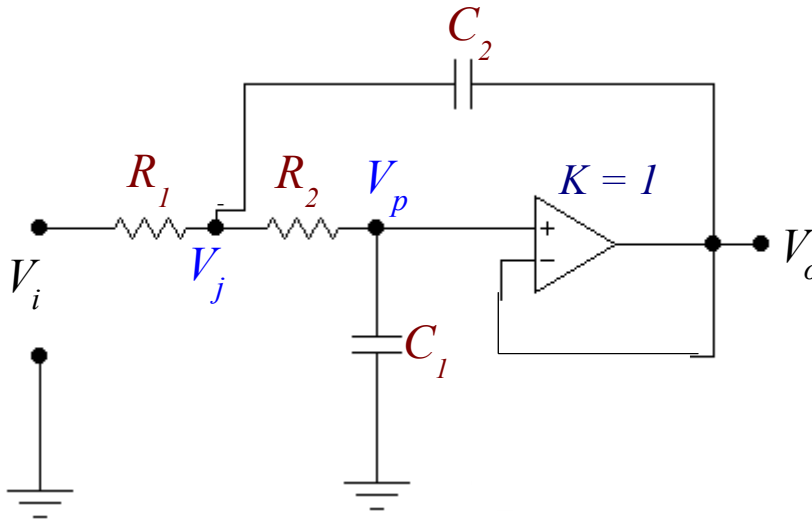
-36.45 dB



205.4 kHz



# Sallen and Key LP Stage with $K = 1$



Recall :  $R_1 C_1 = R_2 C_2 = RC$   
 $\frac{1}{2} \leq Q < \infty \Rightarrow 1 \leq K < 3$

When:  $R_1 C_1 \neq R_2 C_2$   
 we can set  $K = 1$

Note  $K = 1 \Rightarrow K_0 = 1$

$$T(s) = \frac{V_o}{V_i} = \frac{1}{C_1 C_2 R_1 R_2} \frac{1}{s^2 + \left( \frac{1}{C_1 R_1} + \frac{1}{C_1 R_2} \right) s + \frac{1}{C_1 C_2 R_1 R_2}} = \frac{K_0 \omega_0^2}{s^2 + \frac{\omega_0}{Q} s + \omega_0^2}$$



## *Sallen and Key LP Stage with $K = 1$ - cont.*

Normalize frequency and impedance, i.e.  $s_n = \frac{s}{\omega_0}$  and  $Z_n = \frac{Z}{R_0}$

$$G(s_n) = \frac{V_o}{V_i} = \frac{1}{s_n^2 + \left( \frac{1}{C_{1n} R_{1n}} + \frac{1}{C_{1n} R_{2n}} \right) s_n + \frac{1}{C_{1n} C_{2n} R_{1n} R_{2n}}} = \frac{1}{s_n^2 + \frac{1}{Q} s_n + 1}$$

Design Formulas

$$\frac{1}{C_{1n} R_{1n}} + \frac{1}{C_{1n} R_{2n}} = \frac{1}{Q}$$

$$\frac{1}{C_{1n} C_{2n} R_{1n} R_{2n}} = 1$$

Design Formulas (MFM)

$$\frac{1}{C_{1n} R_{1n}} + \frac{1}{C_{1n} R_{2n}} = \sqrt{2}$$

$$\frac{1}{C_{1n} C_{2n} R_{1n} R_{2n}} = 1$$



## Sallen and Key LP Stage with $K = 1$ - cont.

$$\frac{1}{C_{1n} R_{1n}} + \frac{1}{C_{1n} R_{2n}} = \sqrt{2}$$

$$\frac{1}{C_{1n} C_{2n} R_{1n} R_{2n}} = 1$$

Choose  $C_{1n} = 1$  and  $R_{2n} = R_{1n} = R_n$ :

$$\frac{2}{R_n} = \sqrt{2} \Rightarrow R_n = \frac{2}{\sqrt{2}} = \sqrt{2}$$

$$\frac{1}{C_{2n} R_n^2} = 1 \Rightarrow C_{2n} = \frac{1}{R_n^2} = \frac{1}{2}$$

Normalized Design:

$$\begin{aligned} C_{1n} &= 1 \\ C_{2n} &= \frac{1}{2} \\ R_{1n} &= R_{2n} = \sqrt{2} \end{aligned}$$

Denormalized Design:

$$\begin{aligned} C_1 &= \frac{C_{1n}}{\Omega_0 R_0} = \frac{1}{\omega_0 R_0} \\ C_2 &= \frac{1}{2} \frac{1}{\omega_0 R_0} \\ R_1 &= R_2 = \sqrt{2} R_0 \end{aligned}$$



### Comparison

•  $R_1 C_1 = R_2 C_2 = RC$  strategy  $G(s_n) = \frac{K/(R_n C_n)^2}{s_n^2 + \frac{(3-K)}{R_n C_n} s_n + \frac{1}{(R_n C_n)^2}} = \frac{K_0}{s_n^2 + \frac{1}{Q} s_n + 1}$

$$\frac{1}{R_n C_n} = 1$$

$$K = 1 + \frac{R_{fn}}{R_{in}} = 3 - \frac{1}{Q}$$

•  $R_1 C_1 \neq R_2 C_2$  strategy

$$G(s_n) = \frac{V_o}{V_i} = \frac{1}{C_{1n} C_{2n} R_{1n} R_{2n} \left( s_n^2 + \left( \frac{1}{C_{1n} R_{1n}} + \frac{1}{C_{1n} R_{2n}} \right) s_n + \frac{1}{C_{1n} C_{2n} R_{1n} R_{2n}} \right)} = \frac{1}{s_n^2 + \frac{1}{Q} s_n + 1}$$

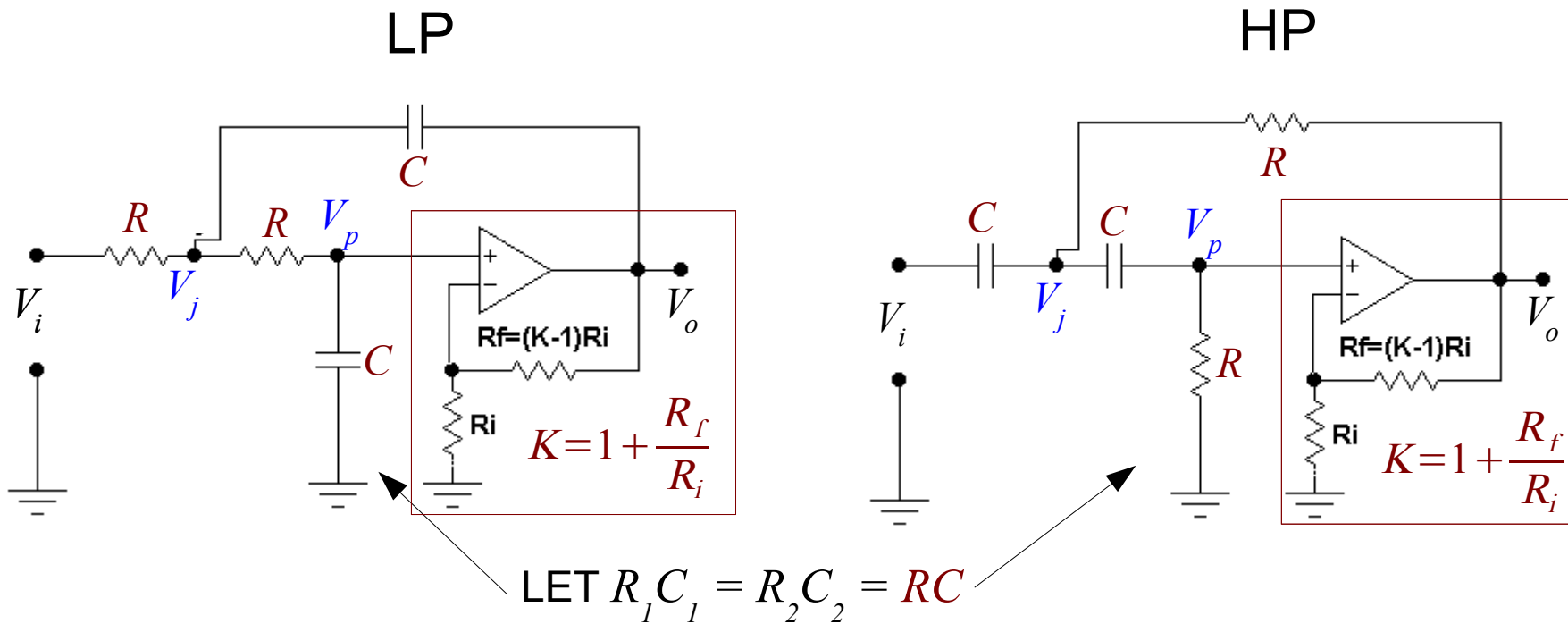
$$\frac{1}{C_{1n} R_{1n}} + \frac{1}{C_{1n} R_{2n}} = \frac{1}{Q} \quad \frac{1}{C_{1n} C_{2n} R_{1n} R_{2n}} = 1$$

$$C_{1n} = 1 \text{ and } R_{2n} = R_{1n} = R_n \Rightarrow \frac{2}{R_n} = \frac{1}{Q} \Rightarrow R_n = 2Q \quad \frac{1}{C_{2n} R_n^2} = 1 \Rightarrow C_{2n} = \frac{1}{R_n^2} = \frac{1}{4Q^2}$$



## Sallen and Key HP Stage

By interchanging 2  $R$ 's and 2  $C$ 's on the LP schematic, we convert an LP circuit to an HP circuit





## Sallen-Key HP Function

Interchanging  $sC$  and  $1/R$  in the LP nodal equations gives:

$$V_j: \frac{V_j - V_i}{R} + sC(V_j - V_o) + \frac{V_j - V_p}{R} = 0 \rightarrow sC(V_j - V_i) + \frac{V_j - V_o}{R} + sC(V_j - V_p) = 0$$

$$V_p: \frac{V_p - V_j}{R} + sC V_p = 0 \rightarrow sC(V_p - V_j) + \frac{V_p}{R} = 0$$

$$V_o = K V_p \rightarrow V_o = K V_p$$

$$G(s) = \frac{V_o}{V_i} = \frac{K s^2}{s^2 + \frac{(3-K)}{CR} s + \left(\frac{1}{CR}\right)^2}$$



## *Sallen-Key HP Function - cont.*

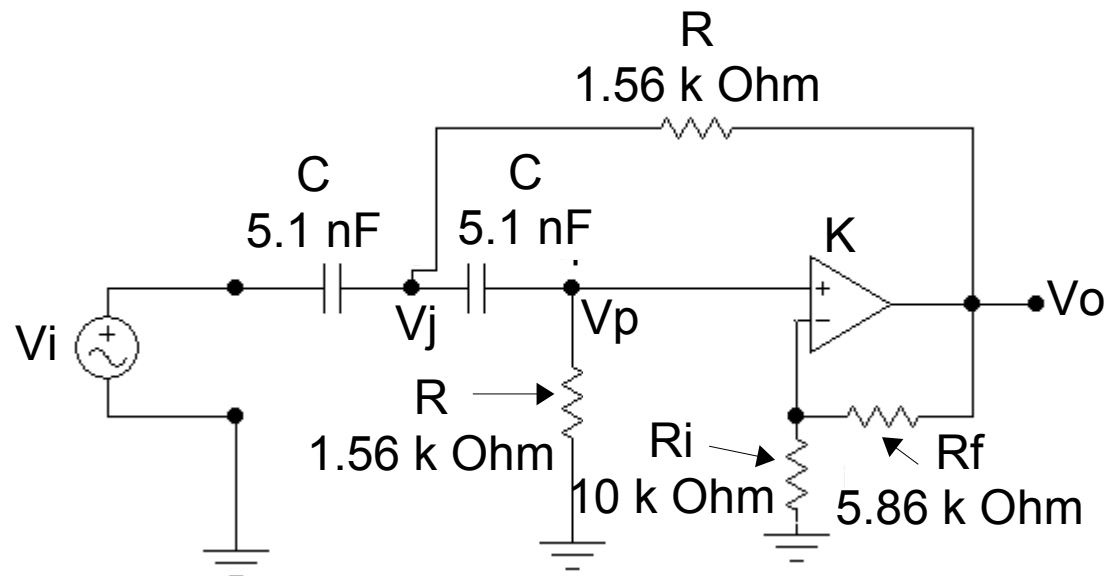
$$G(s) = \frac{V_o}{V_i} = \frac{K s^2}{s^2 + \frac{(3-K)}{CR} s + \left(\frac{1}{CR}\right)^2} = \frac{K_\infty s^2}{s^2 + \frac{\omega_0}{Q} s + \omega_0^2}$$

Note that the HP denominator polynomial (or poles) is the same as for the LP section and the same design equations apply:

$$\omega_0 = \frac{1}{CR} \quad Q = \frac{1}{3-K} \quad K < 3!$$

$$|G(j\infty)| = K_\infty = K$$

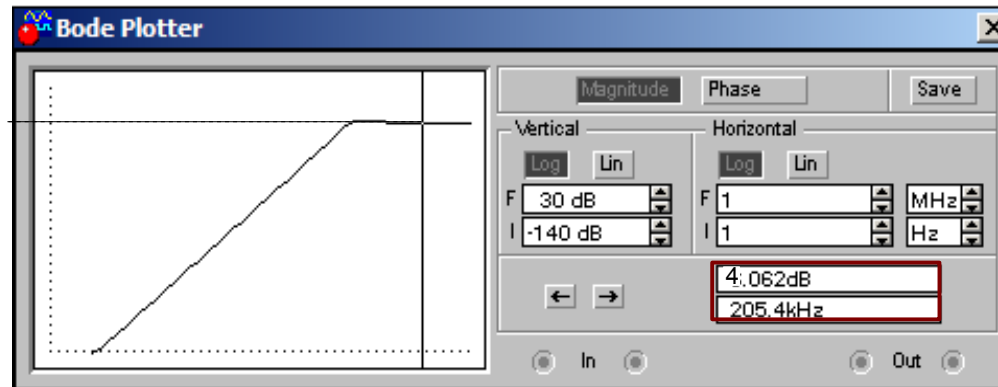
## *20 Khz MFM HP Stage*



## HP Stage Response

Passband  
response

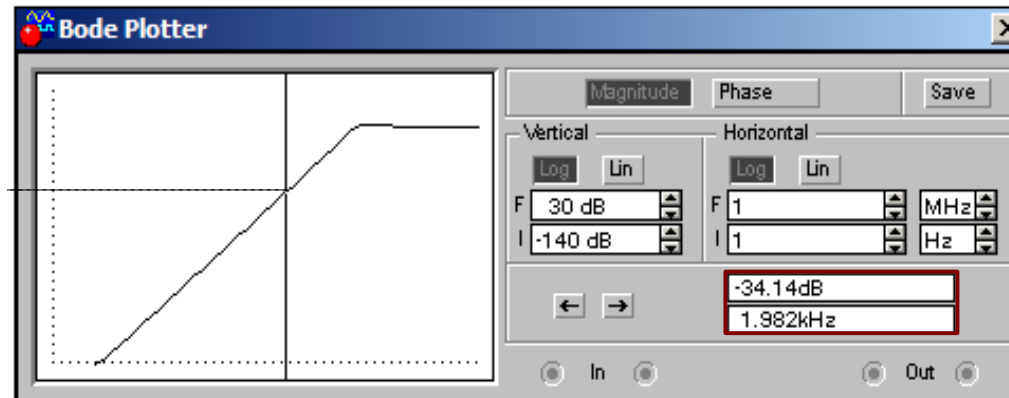
4.06 dB



205.4 kHz

Stopband  
response

-34.14 dB



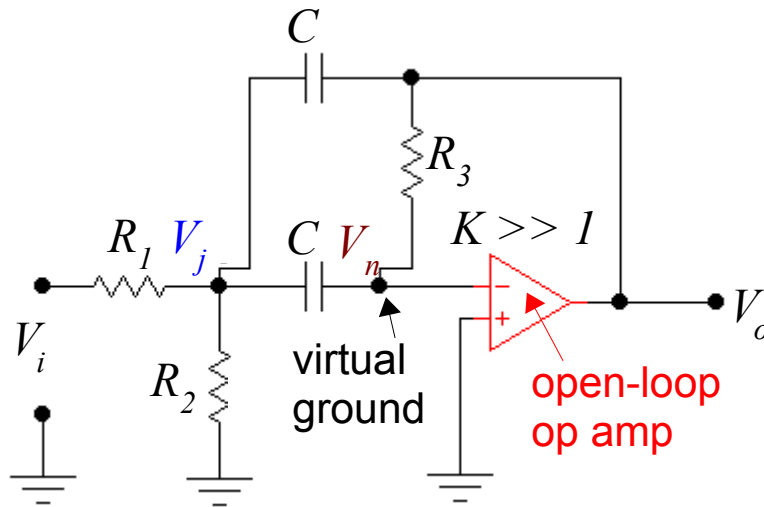
1.98 kHz

## Delyannis-Friend BP Stage

Node Equations:

$$V_j: \frac{V_j - V_i}{R_1} + sC(V_j - V_o) + sC(V_j - V_n) + \frac{V_j}{R_2} = 0$$

Choose  $C_1 = C_2 = C$



$$V_n: sC(V_n - V_j) + \frac{V_n - V_o}{R_3} = 0$$

$$V_o = -K V_n$$

Ideal op amp:  $K \rightarrow \infty \Rightarrow V_n \rightarrow 0$

$$V_o = -K V_n \neq 0$$



## *Delyannis-Friend BP Stage - cont.*

$$G(s) = \frac{V_o}{V_i} = \frac{-\frac{s}{C R_1}}{s^2 + \frac{2}{C R_3} s + \frac{1}{C^2 R_3 \cdot R_1 \parallel R_2}} = \frac{-s \left(\frac{\omega_0}{Q}\right) K_{\omega_0}}{s^2 + \left(\frac{\omega_0}{Q}\right) s + \omega_0^2}$$

Identify:

$$\omega_0^2 = \frac{1}{C^2 R_3 \cdot R_1 \parallel R_2}$$

$$\frac{\omega_0}{Q} = \frac{2}{C R_3}$$

$$K_{\omega_0} = |G(j\omega_0)| = \frac{\omega_0}{C R_1} \frac{C R_3}{2\omega_0} = \frac{R_3}{2 R_1}$$



## *Delyannis-Friend BP Stage - cont.*

$$\omega_0^2 = \frac{1}{C^2 R_3 \cdot R_1 \parallel R_2}$$

$$\frac{\omega_0}{Q} = \frac{2}{C R_3}$$

$$K_{\omega_0} = \frac{R_3}{2 R_1}$$

Given  $\omega_0$ ,  $Q$  and  $K_{\omega_0}$ , choose  $C$  and solve for the resistors:

$$R_3 = \frac{2Q}{C\omega_0} \quad R_1 = \frac{R_3}{2K_{\omega_0}} = \frac{Q}{C\omega_0 K_{\omega_0}}$$

$$R_1 \parallel R_2 = \frac{1}{\omega_0^2 C^2 R_3} = \frac{1}{2\omega_0 C Q}$$

$$R_2 = \frac{R_1}{2\omega_0 C Q R_1 - 1}$$

Normalize  $\omega_{0n} = 1$  and choose  $C_n = 1$ :

$$\boxed{\begin{aligned} R_{3n} &= 2Q & R_{1n} &= \frac{Q}{K_{\omega_0}} & R_{1n} \parallel R_{2n} &= \frac{1}{2Q} \\ R_{2n} &= \frac{R_{1n}}{2QR_{1n} - 1} \end{aligned}}$$

## *Delyannis-Friend BP Stage*

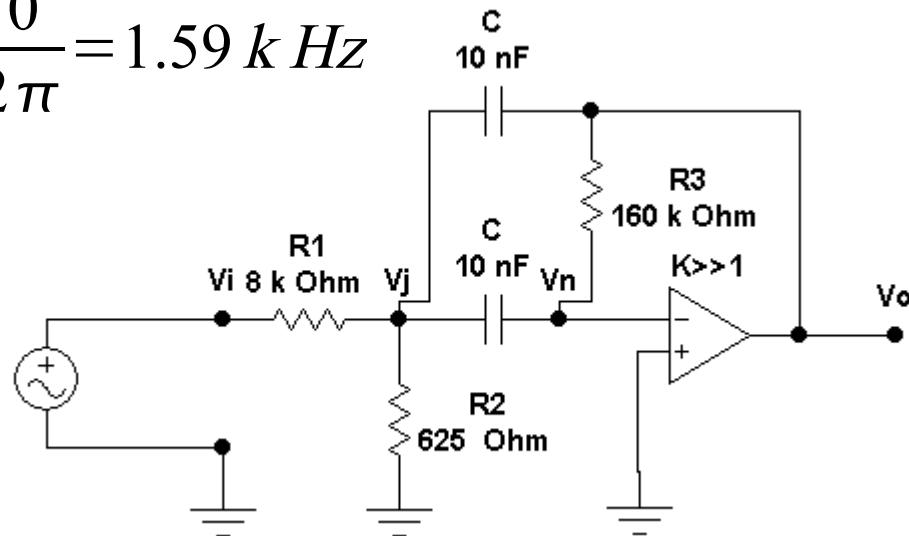
$$\omega_0 = 10^4 \text{ rps} \Rightarrow f_0 = \frac{10^4}{2\pi} = 1.59 \text{ kHz}$$

$$Q = 8$$

$$K_{\omega_0} = 10$$

Choose:

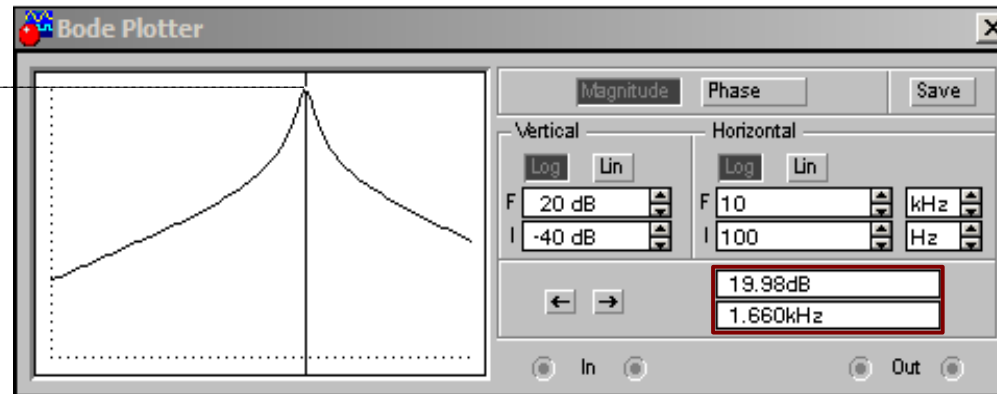
$$C = 10 \text{ nF}$$



## Simulation Results

Peak gain

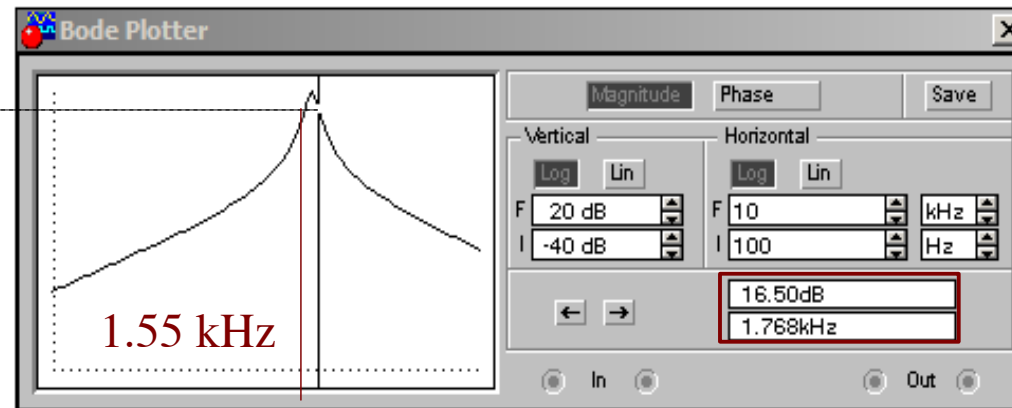
19.98 dB



1.66 kHz

High -3 dB point

16.50 dB



1.77 kHz

$$Q = \frac{1.77 - 1.55}{1.66} = 7.54$$