### ESE 3400: Medical Devices Lab

## Lec 7: November 1, 2023 Digital Filters and Spectral Analysis



# Linear Filter Design

- Used to be an art
  - Now, lots of tools to design optimal filters
- □ For DSP there are two common classes
  - Infinite impulse response IIR
  - Finite impulse response FIR
- □ We will focus on FIR designs



## What is a Linear Filter?

- Attenuates certain frequencies
- Passes certain frequencies
- Affects both phase and magnitude







#### Butterworth

- Monotonic in pass and stop bands
- □ Chebyshev, Type I
  - Equiripple in pass band and monotonic in stop band
- □ Chebyshev, Type II
  - Monotonic in pass band and equiripple in stop band
- Elliptic
  - Equiripple in pass and stop bands







$$X(e^{j\omega}) = \sum_{k=-\infty}^{\infty} x[k]e^{-j\omega k}$$

$$x[n] = \frac{1}{2\pi} \int_{-\pi}^{\pi} X(e^{j\omega}) e^{j\omega n} d\omega$$

## Alternate

$$X(f) = \sum_{k=-\infty}^{\infty} x[k]e^{-j2\pi fk}$$
$$x[n] = \int_{-0.5f_s}^{0.5f_s} X(f)e^{j2\pi fn}df$$









$$W(e^{j\omega}) = \sum_{k=-\infty}^{\infty} w[k]e^{-j\omega k}$$
$$= \sum_{k=-N}^{N} e^{-j\omega k}$$



$$W(e^{j\omega}) = \sum_{k=-N}^{N} e^{-j\omega k}$$

**Useful sum:** 
$$1 + p + p^2 + ... + p^M = \frac{1 - p^{M+1}}{1 - p}$$



$$W(e^{j\omega}) = \sum_{k=-N}^{N} e^{-j\omega k}$$
  
=  $e^{j\omega N} + e^{j\omega(N-1)} + \dots + e^{j\omega 0} + \dots e^{-j\omega(N-1)} + e^{-j\omega N}$   
=  $e^{-j\omega N} (1 + e^{j\omega} + \dots + e^{j\omega N} + \dots + e^{j\omega(2N-1)} + e^{j\omega 2N})$ 

**Useful sum:** 
$$1 + p + p^2 + ... + p^M = \frac{1 - p^{M+1}}{1 - p}$$



$$\begin{split} W(e^{j\omega}) &= \sum_{k=-N}^{N} e^{-j\omega k} \\ &= e^{j\omega N} + e^{j\omega(N-1)} + \dots + e^{j\omega 0} + \dots e^{-j\omega(N-1)} + e^{-j\omega N} \\ &= e^{-j\omega N} \left(1 + e^{j\omega} + \dots + e^{j\omega N} + \dots + e^{j\omega(2N-1)} + e^{j\omega 2N}\right) \end{split}$$

**Useful sum:** 
$$1 + p + p^2 + ... + p^M = \frac{1 - p^{M+1}}{1 - p}$$

$$p = e^{j\omega} \qquad M = 2N$$
$$W(e^{j\omega}) = e^{-j\omega N} \frac{1 - e^{j\omega(2N+1)}}{1 - e^{j\omega}}$$



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$$W(e^{j\omega}) = e^{-j\omega N} \frac{1 - e^{j\omega(2N+1)}}{1 - e^{j\omega}}$$
$$= \frac{e^{-j\omega N} - e^{j\omega(N+1)}}{1 - e^{j\omega}}$$
$$= \frac{e^{-j\omega N} - e^{j\omega(N+1)}}{1 - e^{j\omega}} \times \frac{e^{-j\omega/2}}{e^{-j\omega/2}}$$
$$= \frac{e^{-j\omega(N+1/2)} - e^{j\omega(N+1/2)}}{e^{-j\omega/2} - e^{j\omega/2}} = \frac{\sin\left((N+1/2)\omega\right)}{\sin\left(\omega/2\right)}$$
Periodic sinc









Also, Σw[n]



#### Plot for N=2



## Periodic Sinc









Figure 7.29 Commonly used windows.

## Tradeoff – Ripple vs. Transition Width



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## Hamming





# $\begin{bmatrix} 0 & -20 & -20 & -40$

## Blackman



 Near optimal window quantified as the window maximally concentrated around ω=0

$$w[n] = \begin{cases} \frac{I_0[\beta(1 - [(n - \alpha)/\alpha]^2)^{1/2}]}{I_0(\beta)}, & 0 \le n \le M, \\ 0, & \text{otherwise,} \end{cases}$$

- $\hfill\square$  Two parameters M and  $\beta$
- α=M/2
  I<sub>0</sub>(x) zero<sup>th</sup> order Bessel function of the first kind



**•** M=20





**•** M=20





**β**=6







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**D**(DT)Fourier Transform of impulse response

$$x[n]=e^{j\omega n} \longrightarrow LTI System \rightarrow y[n]=H(e^{j\omega})e^{j\omega n}$$

$$H(e^{j\omega}) = \sum_{k=-\infty}^{\infty} h[k]e^{-j\omega k}$$



Moving Average Filter

• Causal: 
$$M_1=0$$
,  $M_2=M$ 

$$y[n] = \frac{x[n-M] + ... + x[n]}{M+1}$$



Moving Average Filter

• Causal: 
$$M_1=0$$
,  $M_2=M$ 

$$y[n] = \frac{x[n-M] + ... + x[n]}{M+1}$$

Impulse response





Moving Average Filter

• Causal: 
$$M_1=0$$
,  $M_2=M$ 

$$y[n] = \frac{x[n - M] + ... + x[n]}{M + 1}$$











$$w[n] \leftrightarrow W(e^{j\omega}) = \frac{\sin((N+1/2)\omega)}{\sin(\omega/2)}$$



h[n] =





$$w[n] \leftrightarrow W(e^{j\omega}) = \frac{\sin((N+1/2)\omega)}{\sin(\omega/2)}$$

$$h[n] = \frac{1}{M+1} w[n - M/2] \Leftrightarrow H(e^{j\omega}) = 0$$



$$w[n] \Leftrightarrow W(e^{j\omega}) = \frac{\sin((N+1/2)\omega)}{\sin(\omega/2)}$$

$$h[n] = \frac{1}{M+1} w[n - M/2] \Leftrightarrow H(e^{j\omega}) = 0$$

$$x[n-n_d] \Leftrightarrow e^{-j\omega n_d} X(e^{j\omega})$$

33



$$w[n] \stackrel{\text{``window''}}{\underset{N}{\circ} \circ \underset{N}{\circ} \circ \underset{$$

h[n]





M=4 (N=2)

$$H(e^{j\omega}) = \frac{e^{-j\omega M/2}}{M+1} \frac{\sin\left((M/2 + 1/2)\omega\right)}{\sin\left(\omega/2\right)}$$



The frequency response H(ω) of the ideal low-pass filter passes low frequencies (near ω = 0) but blocks high frequencies (near ω = ±π)

$$H(\omega) = \begin{cases} 1 & -\omega_c \le \omega \le \omega_c \\ 0 & \text{otherwise} \end{cases}$$




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$$H(\omega) = \begin{cases} 1 & -\omega_c \le \omega \le \omega_c \\ 0 & \text{otherwise} \end{cases}$$



 $\blacksquare$  Compute the impulse response h[n] given this  $H(\omega)$ 

Apply the inverse DTFT

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$$h[n] = \int_{-\pi}^{\pi} H(\omega) e^{j\omega n} \frac{d\omega}{2\pi} = \int_{-\omega_c}^{\omega_c} e^{j\omega n} \frac{d\omega}{2\pi} = \left. \frac{e^{j\omega n}}{2\pi jn} \right|_{-\omega_c}^{\omega_c} = \frac{e^{j\omega_c n} - e^{-j\omega_c n}}{2\pi jn} = \frac{\omega_c}{\pi} \frac{\sin(\omega_c n)}{\omega_c n}$$



The frequency response H(ω) of the ideal low-pass filter passes low frequencies (near ω = 0) but blocks high frequencies (near ω = ±π)

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The frequency response H(ω) of the ideal low-pass filter passes low frequencies (near ω = 0) but blocks high frequencies (near ω = ±π)







□ Pass band smeared and rippled

- Smearing determined by width of main lobe
- Rippling determined by size of side lobes



• With multiplication in time property,

$$h_{LP}[n] = w_N[n-N] \cdot h[n-N]$$

$$H(e^{j\omega}) = H_d(e^{j\omega}) * W(e^{j\omega})$$





□ With multiplication in time property,

$$H(e^{j\omega}) = H_d(e^{j\omega}) * W(e^{j\omega})$$

□ For Boxcar (rectangular) window













- Choose a desired frequency response  $H_d(e^{j\omega})$ 
  - non causal (zero-delay), and infinite imp. response
  - If derived from C.T, choose T and use:

$$H_d(e^{j\omega}) = H_c(j\frac{\Omega}{T})$$

- Window:
  - Length  $M+1 \Leftrightarrow$  affects transition width
  - Type of window ⇔ transition-width/ ripple



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- Window:
  - Length  $M+1 \Leftrightarrow$  affects transition width
  - Type of window ⇔ transition-width/ ripple
  - Modulate to shift impulse response
    - Force causality

$$H_d(e^{j\omega})e^{-j\omega\frac{M}{2}}$$



• Determine truncated impulse response  $h_1[n]$ 

$$h_1[n] = \begin{cases} \frac{1}{2\pi} \int_{-\pi}^{\pi} H_d(e^{j\omega}) e^{-j\omega \frac{M}{2}} e^{j\omega n} & 0 \le n \le M \\ 0 & \text{otherwise} \end{cases}$$

• Apply window

$$h_w[n] = w[n]h_1[n]$$

• Check:

Compute H<sub>w</sub>(e<sup>jω</sup>), if does not meet specs increase M or change window



$$H_d(e^{j\omega}) = \begin{cases} 1 & |\omega| \le \omega_c \\ 0 & \text{otherwise} \end{cases}$$

Choose  $M \Rightarrow$  Window length and set

$$H_1(e^{j\omega}) = H_d(e^{j\omega})e^{-j\omega\frac{M}{2}}$$

$$h_1[n] = \begin{cases} \frac{\sin(\omega_c(n-M/2))}{\pi(n-M/2)} & 0 \le n \le M \\ 0 & \text{otherwise} \end{cases}$$

$$\frac{\omega_c}{\pi}\operatorname{sinc}(\frac{\omega_c}{\pi}(n-M/2))$$



□ The result is a windowed sinc function

$$h_w[n] = w[n]h_1[n]$$
$$\underbrace{\frac{\omega_c}{\pi}\operatorname{sinc}}_{\pi}(\frac{\omega_c}{\pi}(n - M/2))$$



- Window method
  - Design Filters heuristically using windowed sinc functions
  - Choose order and window type
  - Check DTFT to see if filter specs are met
- Optimal design
  - Design a filter h[n] with  $H(e^{j\omega})$
  - Approximate H<sub>d</sub>(e<sup>jω</sup>) with some optimality criteria or satisfies specs.



□ Least Squares:

minimize 
$$\int_{\omega \in \text{care}} |H(e^{j\omega}) - H_d(e^{j\omega})|^2 d\omega$$

Variation: Weighted Least Squares:

minimize 
$$\int_{-\pi}^{\pi} W(\omega) |H(e^{j\omega}) - H_d(e^{j\omega})|^2 d\omega$$

# Spectral Analysis Using the DFT

- **•** Two important tools:
  - Applying a window  $\rightarrow$  reduced artifacts
  - Zero-padding  $\rightarrow$  increases spectral sampling

Parameter	Symbol	Units
Sampling interval	Т	S
Sampling frequency	$\Omega_{s}=rac{2\pi}{T}$	rad/s
Window length	L	unitless
Window duration	$L \cdot T$	S
DFT length	$N \ge L$	unitless
DFT duration	$N \cdot T$	S
Spectral resolution	$\frac{\Omega_s}{L} = \frac{2\pi}{L \cdot T}$	rad/s
Spectral sampling interval	$\frac{\overline{\Omega_s}}{N} = \frac{2\pi}{N \cdot T}$	rad/s



$$\begin{split} x_c(t) &= A_1 \cos(\omega_1 t) + A_2 \cos(\omega_2 t) \\ X_c(j\Omega) &= A_1 \pi \Big[ \delta(\Omega - \omega_1) + \delta(\Omega + \omega_1) \Big] + A_2 \pi \Big[ \delta(\Omega - \omega_2) + \delta(\Omega + \omega_2) \Big] \end{split}$$



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FT of Original CT Signal (heights represent areas of  $\delta(\Omega)$  impulses)





If we sample the signal over an infinite time duration, we would have:

$$x[n] = x_{c}(t)\Big|_{t=nT}, \quad -\infty < n < \infty$$

□ With the discrete time Fourier transform (DTFT):

$$X(e^{j\Omega T}) = \frac{1}{T} \sum_{r=-\infty}^{\infty} X_c \left( j \left( \Omega - r \frac{2\pi}{T} \right) \right), \quad -\infty < \Omega < \infty$$



$$\begin{split} x_c(t) &= A_1 \cos(\omega_1 t) + A_2 \cos(\omega_2 t) \\ X_c(j\Omega) &= A_1 \pi \Big[ \delta(\Omega - \omega_1) + \delta(\Omega + \omega_1) \Big] + A_2 \pi \Big[ \delta(\Omega - \omega_2) + \delta(\Omega + \omega_2) \Big] \end{split}$$



FT of Original CT Signal (heights represent areas of  $\delta(\Omega)$  impulses)





• Sampling with  $\Omega s/2\pi = 1/T = 20Hz$ 







 In any real system, we sample only over a finite block of L samples:

$$x[n] = x_{c}(t) \Big|_{t=nT}, \quad 0 < n < L-1$$

- This simply corresponds to a rectangular window of duration L
- Recall there are many other window types
  - Hann, Hamming, Blackman, Kaiser, etc.







We take the block of signal samples and multiply by a window of duration L, obtaining:

$$v[n] = x[n] \cdot w[n], \quad 0 < n < L-1$$

If the window w[n] has DTFT, W(e<sup>jω</sup>), then the windowed block of signal samples has a DTFT given by the periodic convolution between X(e<sup>jω</sup>) and W(e<sup>jω</sup>):

$$V(e^{j\omega}) = \frac{1}{2\pi} \int_{-\pi}^{\pi} X(e^{j\theta}) W(e^{j(\omega-\theta)}) d\theta$$

# Windowed Sampled CT Signal

- Convolution with W(e<sup>jω</sup>) has two effects in the spectrum:
  - It limits the spectral resolution (spectral spreading)
    - Main lobes of the DTFT of the window
  - The window can produce spectral leakage
    - Side lobes of the DTFT of the window
- These two are always a tradeoff
  time-frequency uncertainty principle



• Sampling with  $\Omega s/2\pi = 1/T = 20Hz$ 





- As before, the sampling rate is  $\Omega s/2\pi = 1/T = 20Hz$
- □ Rectangular Window, L = 32



•

- As before, the sampling rate is  $\Omega s/2\pi = 1/T = 20Hz$
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•

•



- As before, the sampling rate is  $\Omega s/2\pi = 1/T = 20Hz$
- □ Rectangular Window, L = 32



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•

• As before, the sampling rate is  $\Omega s/2\pi = 1/T = 20Hz$ 

□ Triangular Window, L = 32

•



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- As before, the sampling rate is  $\Omega s/2\pi = 1/T = 20Hz$
- □ Hamming Window, L = 32



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- As before, the sampling rate is  $\Omega s/2\pi = 1/T = 20Hz$
- □ Hamming Window, L = 64









 $y[n] = \sin(2\pi 0.1992n) + 0.005\sin(2\pi 0.25n) | 0 \le n \le 128$ 



#### Window Comparison Example



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In preparation for taking an N-point DFT, we may zero-pad the windowed block of signal samples

$$\begin{cases} v[n] & 0 \le n \le L - 1 \\ 0 & L \le n \le N - 1 \end{cases}$$

- This zero-padding has no effect on the DTFT of v[n], since the DTFT is computed by summing over infinity
- Effect of Zero Padding

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 We take the N-point DFT of the zero-padded v[n], to obtain the block of N spectral samples:


## • Hamming window, L = N = 32





Spectrum of Sampled, Windowed, Zero-Padded Signal



N-Point DFT of Sampled, Windowed, Zero-Padded Signal



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## • Hamming window, L = 32, Zero-padded to N = 64

|V[k]|

k

Sampled, Windowed Signal, Hamming Window, L = 32, Zero-Padded to N = 64

N-Point DFT of Sampled, Windowed, Zero-Padded Signal



Spectrum of Sampled, Windowed, Zero-Padded Signal





## Frequency Analysis with DFT

- Length of window determines spectral resolution
- Type of window determines side-lobe amplitude/main-lobe width (spectral leakage/spreading)
  - Some windows have better tradeoff between resolution and side-lobe height
- Zero-padding approximates the DTFT better (spectral sampling). Does not introduce new information!



- Finish Lab 8 by Monday
- □ Lab 9 on Monday
  - More digital filters