

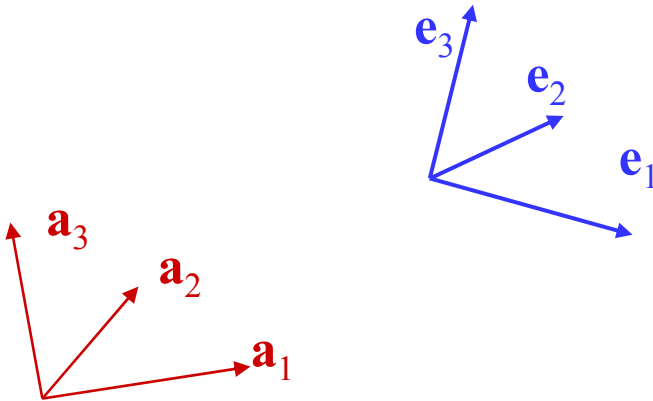
Kinematics



Scalar and Vector Functions

$\phi(q_1, q_2, \dots, q_n)$ is a scalar function of n variables

$\phi(q_1, q_2, \dots, q_n)$ is independent of reference frames – scalar invariant



NB: No assumptions of orthogonality!

$\mathbf{v}(q_1, q_2, \dots, q_n)$ is a vector function \mathbf{v} of n variables.

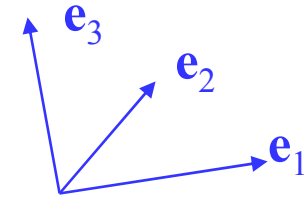
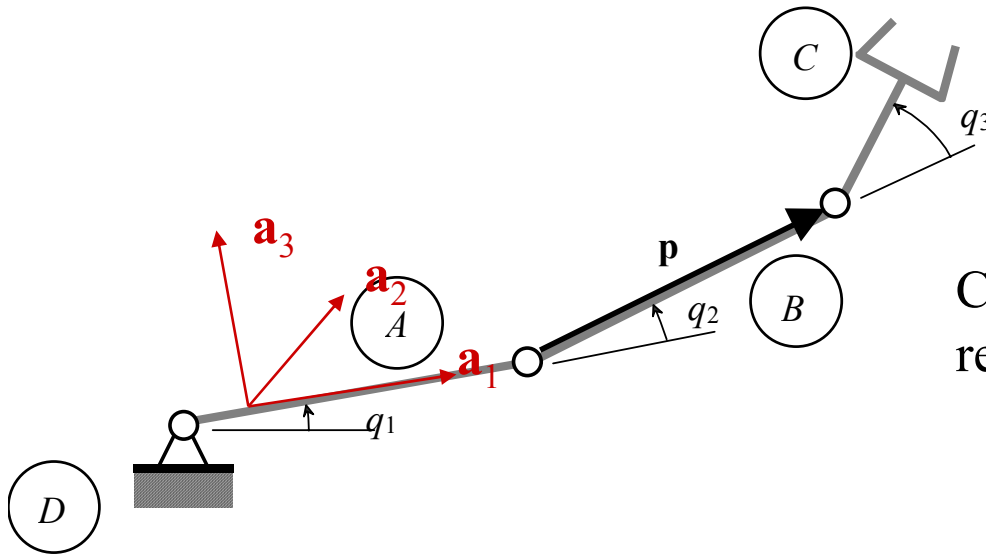
In any reference frame $\{A\}$, we can find three independent vectors \mathbf{a}_1 , \mathbf{a}_2 , and \mathbf{a}_3 that are basis vectors.

The vector function $\mathbf{v}(q_1, q_2, \dots, q_n)$ can be expressed as a linear combination of the three vectors:

$$\mathbf{v}(q_1, q_2, \dots, q_n) = v_1(q_1, q_2, \dots, q_n) \mathbf{a}_1 + v_2(q_1, q_2, \dots, q_n) \mathbf{a}_2 + v_3(q_1, q_2, \dots, q_n) \mathbf{a}_3$$

The three coefficients are the three scalar functions v_1 , v_2 , and v_3 . They are called *components* and these three functions are unique once the vectors \mathbf{a}_1 , \mathbf{a}_2 , and \mathbf{a}_3 are specified.

Reference Frames



Components of vectors depend on the reference triad

$$\mathbf{p} = p_1 \mathbf{e}_1 + p_2 \mathbf{e}_2 + p_3 \mathbf{e}_3,$$

$$\mathbf{v} = v_1 \mathbf{e}_1 + v_2 \mathbf{e}_2 + v_3 \mathbf{e}_3,$$

$${}^E[\mathbf{p}] = \begin{bmatrix} p_1 \\ p_2 \\ p_3 \end{bmatrix}, \quad {}^E[\mathbf{v}] = \begin{bmatrix} v_1 \\ v_2 \\ v_3 \end{bmatrix}$$

A robotic arm is a system of rigid bodies (reference frames) A , B , and C . D is the inertial or the laboratory reference frame that is considered fixed.

$${}^E[\mathbf{p}] \neq {}^A[\mathbf{p}]$$

Standard Reference Triad

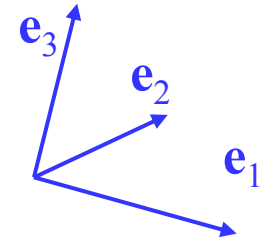
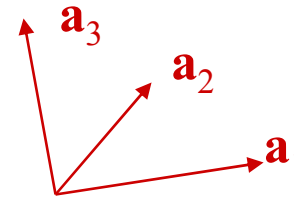
Three vectors rigidly attached to a reference frame satisfying the equations below constitute a **standard reference triad** or simply a reference triad.

$$\mathbf{a}_i \cdot \mathbf{a}_j = \begin{cases} 0, & i \neq j \\ 1, & i = j \end{cases}$$

$$\mathbf{a}_1 \times \mathbf{a}_2 = \mathbf{a}_3,$$

$$\mathbf{a}_2 \times \mathbf{a}_3 = \mathbf{a}_1,$$

$$\mathbf{a}_3 \times \mathbf{a}_1 = \mathbf{a}_2$$



- Projection rule

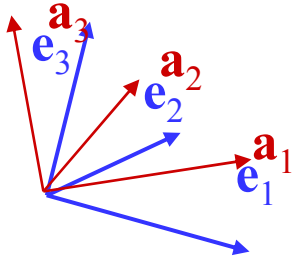
$$\mathbf{u} \cdot \mathbf{e}_i = u_i$$

- Composition rule

$$\mathbf{u} = \sum_{i=1}^3 (\mathbf{u} \cdot \mathbf{e}_i) \mathbf{e}_i$$

$$\mathbf{u} = u_1 \mathbf{e}_1 + u_2 \mathbf{e}_2 + u_3 \mathbf{e}_3 = \sum_{i=1}^3 u_i \mathbf{e}_i$$

Transformation of Vectors



Components in $\{A\}$ and in $\{E\}$ are related by:

$${}^E[\mathbf{p}]_i = \sum_j (\mathbf{e}_i \cdot \mathbf{a}_j) {}^A[\mathbf{p}]_j$$

$$\sum_i {}^E[\mathbf{p}]_i \mathbf{e}_i = \sum_j {}^A[\mathbf{p}]_j \mathbf{a}_j$$

$$\begin{aligned} {}^E[\mathbf{p}] &= [{}^E \mathbf{R}_A] {}^A[\mathbf{p}] \\ &= \begin{bmatrix} \mathbf{e}_1 \cdot \mathbf{a}_1 & \mathbf{e}_1 \cdot \mathbf{a}_2 & \mathbf{e}_1 \cdot \mathbf{a}_3 \\ \mathbf{e}_2 \cdot \mathbf{a}_1 & \mathbf{e}_2 \cdot \mathbf{a}_2 & \mathbf{e}_2 \cdot \mathbf{a}_3 \\ \mathbf{e}_3 \cdot \mathbf{a}_1 & \mathbf{e}_3 \cdot \mathbf{a}_2 & \mathbf{e}_3 \cdot \mathbf{a}_3 \end{bmatrix} {}^A[\mathbf{p}] \end{aligned}$$

Rotation matrix that transforms components in $\{A\}$ into components in $\{E\}$

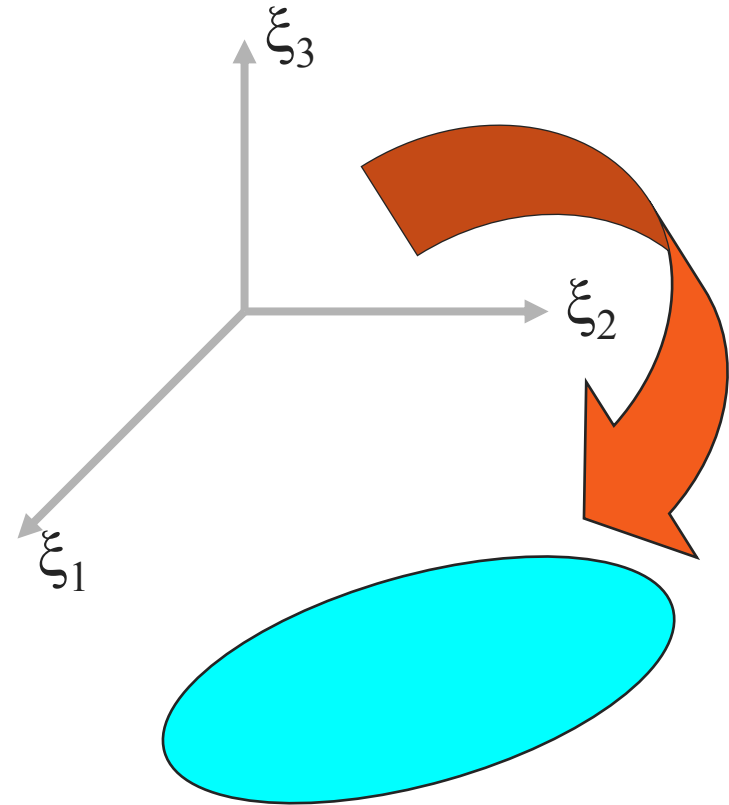
Rotation Matrices



Properties of Rotation Matrices

- Orthogonal
 - ◆ Matrix times its transpose equals 1
- Special orthogonal
 - ◆ Determinant is +1
- Closed under multiplication
- Composition

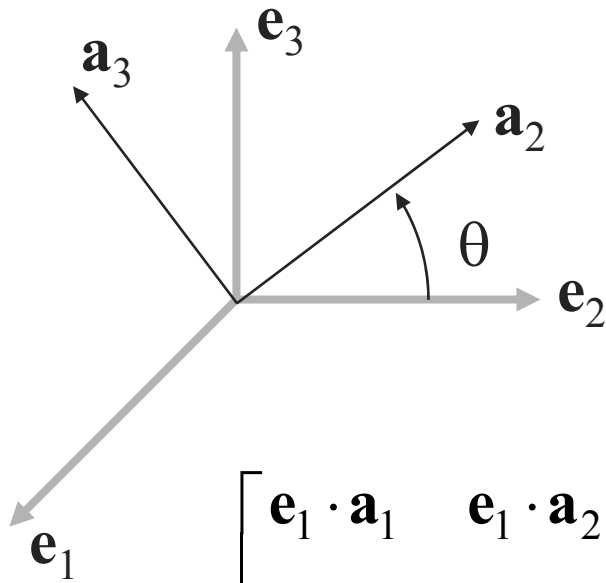
$${}^A\mathbf{R}_C = {}^A\mathbf{R}_B \times {}^B\mathbf{R}_C$$
- The inverse of a rotation matrix is also a rotation matrix
- Composition and inverse operations are “continuous functions”
- The set of all rotations is a *Lie Group*, $SO(3)$
- $SO(3)$ can be parameterized by 3 coordinates



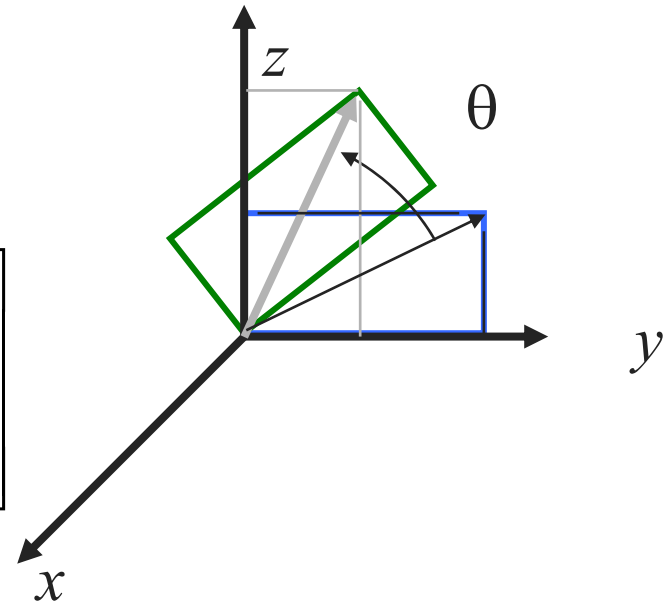
Example: “Simple” Rotations

- Rotation about the x -axis through θ

$$Rot(x, \theta) = \begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos \theta & -\sin \theta \\ 0 & \sin \theta & \cos \theta \end{bmatrix}$$

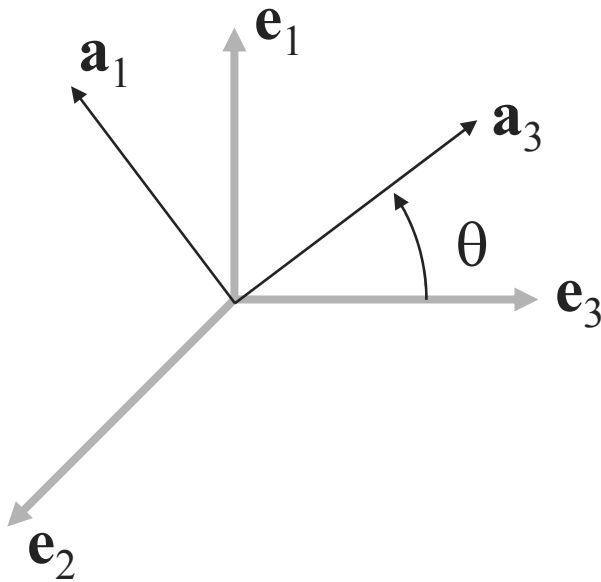


$$\begin{bmatrix} \mathbf{e}_1 \cdot \mathbf{a}_1 & \mathbf{e}_1 \cdot \mathbf{a}_2 & \mathbf{e}_1 \cdot \mathbf{a}_3 \\ \mathbf{e}_2 \cdot \mathbf{a}_1 & \mathbf{e}_2 \cdot \mathbf{a}_2 & \mathbf{e}_2 \cdot \mathbf{a}_3 \\ \mathbf{e}_3 \cdot \mathbf{a}_1 & \mathbf{e}_3 \cdot \mathbf{a}_2 & \mathbf{e}_3 \cdot \mathbf{a}_3 \end{bmatrix}$$



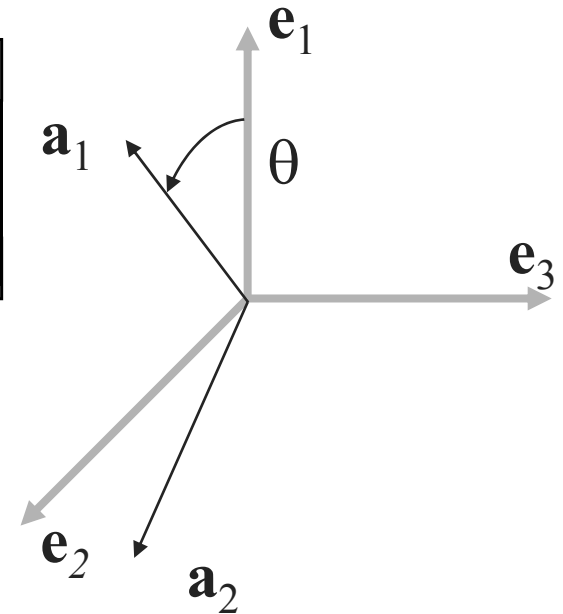
Example: Rotation

Rotation about the y -axis through θ



$$\begin{bmatrix} \mathbf{e}_1 \cdot \mathbf{a}_1 & \mathbf{e}_1 \cdot \mathbf{a}_2 & \mathbf{e}_1 \cdot \mathbf{a}_3 \\ \mathbf{e}_2 \cdot \mathbf{a}_1 & \mathbf{e}_2 \cdot \mathbf{a}_2 & \mathbf{e}_2 \cdot \mathbf{a}_3 \\ \mathbf{e}_3 \cdot \mathbf{a}_1 & \mathbf{e}_3 \cdot \mathbf{a}_2 & \mathbf{e}_3 \cdot \mathbf{a}_3 \end{bmatrix}$$

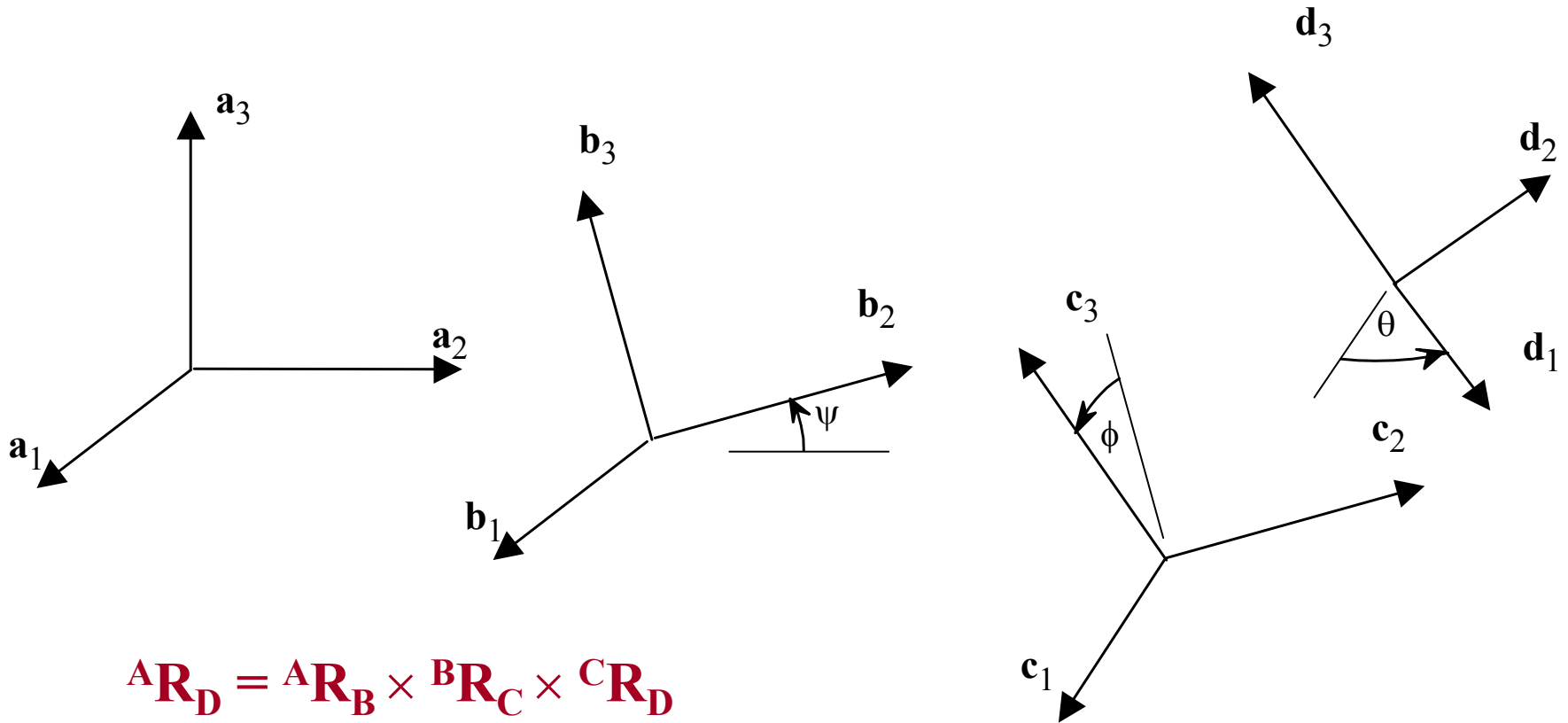
Rotation about the z -axis through θ



$$Rot(y, \theta) = \begin{bmatrix} \cos \theta & 0 & \sin \theta \\ 0 & 1 & 0 \\ -\sin \theta & 0 & \cos \theta \end{bmatrix}$$

$$Rot(z, \theta) = \begin{bmatrix} \cos \theta & -\sin \theta & 0 \\ \sin \theta & \cos \theta & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

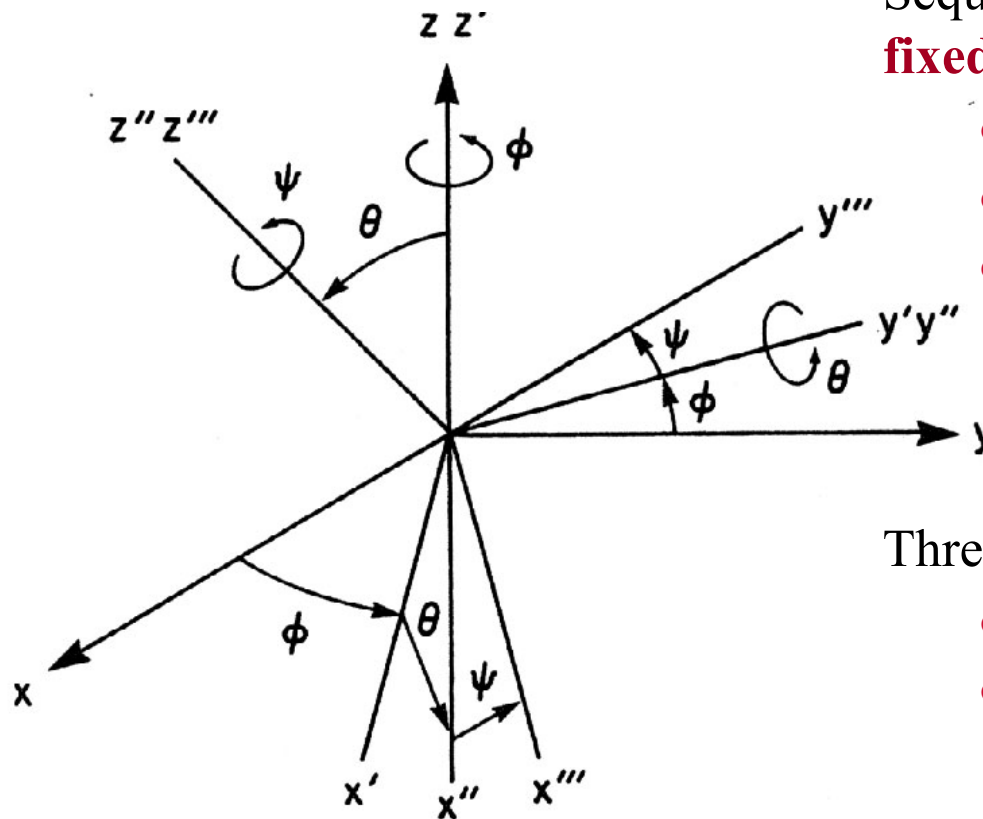
Composition of Three Rotations



$${}^A\mathbf{R}_D = {}^A\mathbf{R}_B \times {}^B\mathbf{R}_C \times {}^C\mathbf{R}_D$$

$${}^A\mathbf{R}_D = \text{Rot}(z, \phi) \times \text{Rot}(y, \theta) \times \text{Rot}(z, \psi)$$

Euler Angles: Parameterization of Rotation Matrices



Sequence of three rotations about **body-fixed** axes

- Rot(z, ϕ)
- Rot(y, θ)
- Rot(z, ψ)

Three Euler Angles

- $\phi, \theta,$ and ψ
- Parameterize rotations

Note

- $\theta = 0$ is a special (singular) case

$$\mathbf{R} = \text{Rot}(z, \phi) \times \text{Rot}(y, \theta) \times \text{Rot}(z, \psi)$$

Determination of Euler Angles

$$\mathbf{R} = \text{Rot}(z, \phi) \times \text{Rot}(y, \theta) \times \text{Rot}(z, \psi)$$

$$R := \begin{bmatrix} \cos(\phi) \cos(\theta) \cos(\psi) - \sin(\phi) \sin(\psi) & -\cos(\phi) \cos(\theta) \sin(\psi) - \sin(\phi) \cos(\psi) & \cos(\phi) \sin(\theta) \\ \sin(\phi) \cos(\theta) \cos(\psi) + \cos(\phi) \sin(\psi) & -\sin(\phi) \cos(\theta) \sin(\psi) + \cos(\phi) \cos(\psi) & \sin(\phi) \sin(\theta) \\ -\sin(\theta) \cos(\psi) & \sin(\theta) \sin(\psi) & \cos(\theta) \end{bmatrix}$$

$$R_{13} = -\sin \theta \cos \psi$$

$$R_{23} = \sin \theta \sin \psi$$

$$\begin{bmatrix} R_{1,1} & R_{1,2} & R_{1,3} \\ R_{2,1} & R_{2,2} & R_{2,3} \\ R_{3,1} & R_{3,2} & R_{3,3} \end{bmatrix}$$

$$R_{33} = \cos \theta$$

$$R_{13} = \sin \theta \cos \phi$$

$$R_{23} = \sin \theta \sin \phi$$

Position, Velocity, Angular Velocity and Acceleration Vectors



Position, Velocity and Acceleration Vectors

\mathbf{p} is a position vector of P in A

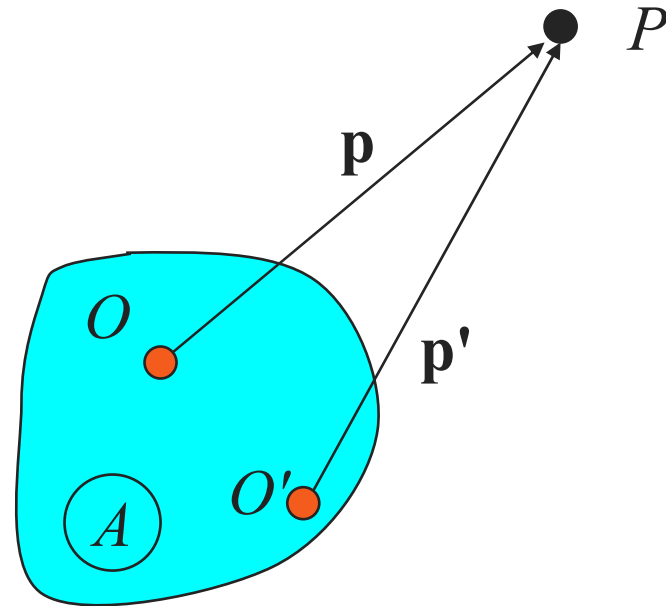
- Emanates from a point fixed to A
- Ends up at P

${}^A\mathbf{v}^P$ is the velocity of P in A

$${}^A\mathbf{v}^P = \frac{{}^A d\mathbf{p}}{dt}$$

${}^A\mathbf{a}^P$ is the acceleration of P in A

$${}^A\mathbf{a}^P = \frac{{}^A d\left({}^A\mathbf{v}^P\right)}{dt}$$



What if a different position vector were chosen?

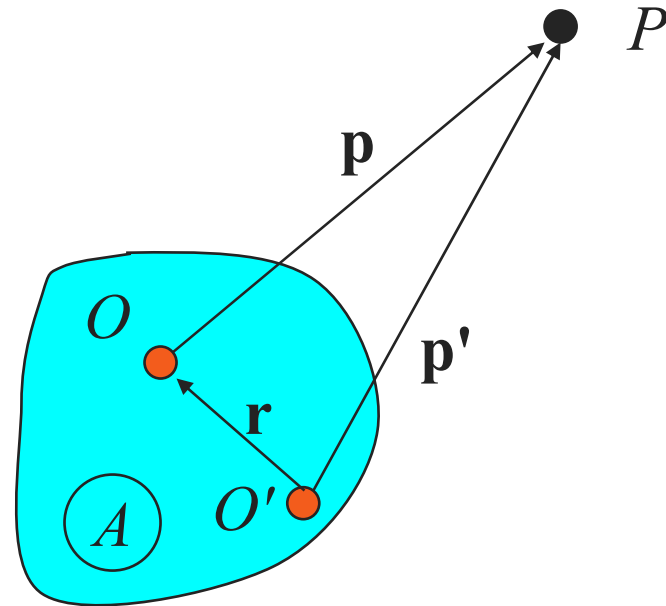
Velocity of P in A is independent of choice of “origin” in A !

\mathbf{p} is a position vector of P in A

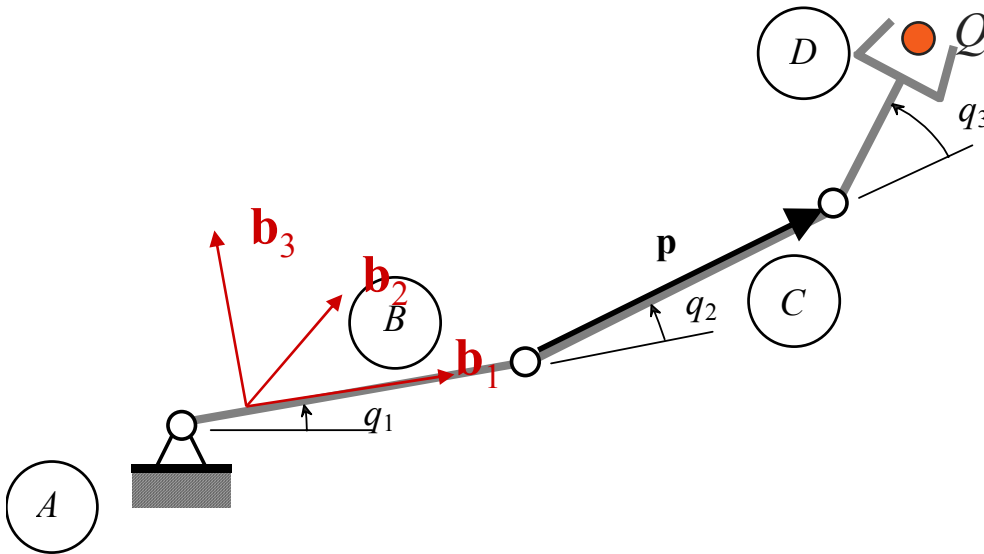
- Emanates from a point fixed to A
- Ends up at P

${}^A\mathbf{v}^P$ is the velocity of P in A

$$\begin{aligned} {}^A\mathbf{v}^P &= \frac{{}^A d\mathbf{p}'}{dt} \\ &= \frac{{}^A d(\mathbf{p} + \mathbf{r})}{dt} \end{aligned}$$



Example



1. Are the following equal?

$$\frac{\partial \mathbf{p}}{\partial q_2} \quad \frac{{}^A \partial \mathbf{p}}{\partial q_2} \quad \frac{{}^B \partial \mathbf{p}}{\partial q_2} \quad \frac{{}^C \partial \mathbf{p}}{\partial q_2}$$

2. If motor (joint) rates are given, calculate $\frac{{}^A d\mathbf{p}}{dt}$

$$\frac{{}^A d\mathbf{p}}{dt} = \frac{{}^A \partial \mathbf{p}}{\partial q_1} \dot{q}_1 + \frac{{}^A \partial \mathbf{p}}{\partial q_2} \dot{q}_2 + \frac{{}^A \partial \mathbf{p}}{\partial q_3} \dot{q}_3$$

3. Find the velocity of Q in A

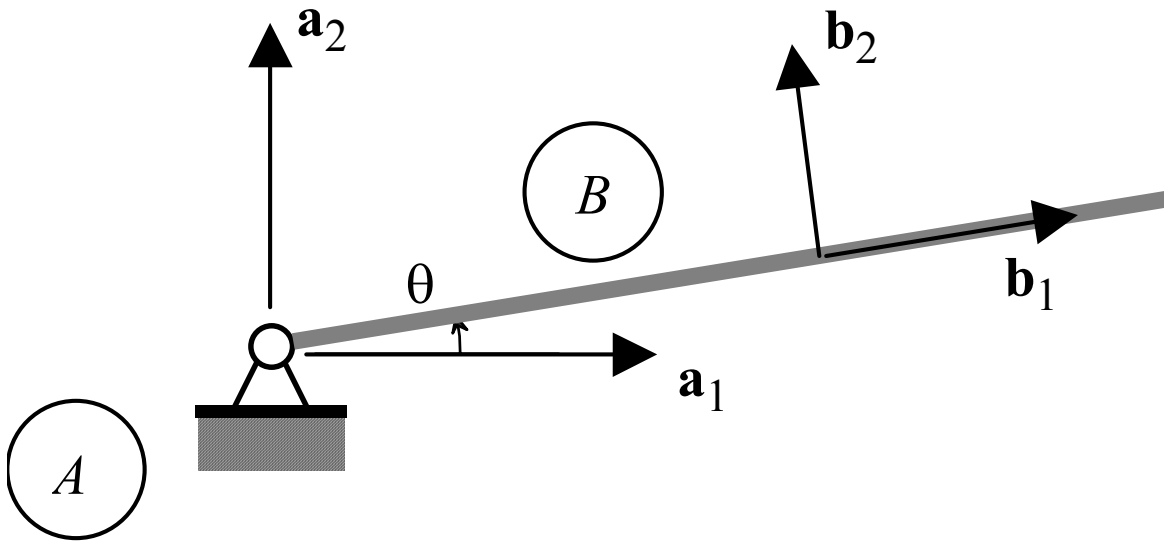
A robotic arm is a system of rigid bodies (reference frames) B , C , and D . A is the inertial or the laboratory reference frame that is considered fixed.

Angular Velocity (Kane)

The *angular velocity of B in A*, denoted by ${}^A\boldsymbol{\omega}^B$, is defined as:

$${}^A\boldsymbol{\omega}^B = \mathbf{b}_1 \left(\frac{{}^A d\mathbf{b}_2}{dt} \cdot \mathbf{b}_3 \right) + \mathbf{b}_2 \left(\frac{{}^A d\mathbf{b}_3}{dt} \cdot \mathbf{b}_1 \right) + \mathbf{b}_3 \left(\frac{{}^A d\mathbf{b}_1}{dt} \cdot \mathbf{b}_2 \right)$$

- Defined in terms of a reference triad attached to B
- *Independent* of reference triad attached to A
- Generalizes to three dimensions
- Yields simple results for derivatives of vectors



Example

$$\mathbf{b}_1 = \mathbf{a}_1 \cos \theta + \mathbf{a}_2 \sin \theta$$

$$\mathbf{b}_2 = \mathbf{a}_2 \cos \theta - \mathbf{a}_1 \sin \theta$$

Differentiation of vectors

1. Vector fixed to B

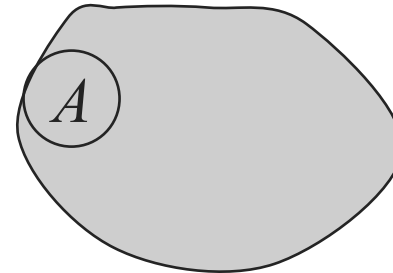
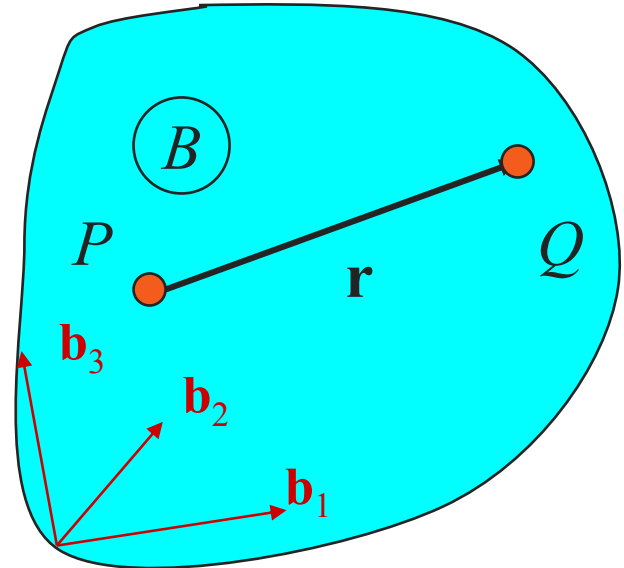
$$\mathbf{r} = r_1 \mathbf{b}_1 + r_2 \mathbf{b}_2 + r_3 \mathbf{b}_3$$

$$\frac{{}^A d\mathbf{r}}{dt} = r_1 \frac{{}^A d\mathbf{b}_1}{dt} + r_2 \frac{{}^A d\mathbf{b}_2}{dt} + r_3 \frac{{}^A d\mathbf{b}_3}{dt}$$

Composition and Projection rule

$$\frac{{}^A d\mathbf{b}_1}{dt} = \left(\frac{{}^A d\mathbf{b}_1}{dt} \cdot \mathbf{b}_1 \right) \mathbf{b}_1 + \left(\frac{{}^A d\mathbf{b}_1}{dt} \cdot \mathbf{b}_2 \right) \mathbf{b}_2 + \left(\frac{{}^A d\mathbf{b}_1}{dt} \cdot \mathbf{b}_3 \right) \mathbf{b}_3$$

$$- \left(\mathbf{b}_1 \cdot \frac{{}^A d\mathbf{b}_3}{dt} \right)$$



Differentiation of vectors (cont'd)

$${}^A\omega^B \times \mathbf{b}_1 = \left[\mathbf{b}_1 \left(\frac{{}^A d\mathbf{b}_2}{dt} \cdot \mathbf{b}_3 \right) + \mathbf{b}_2 \left(\frac{{}^A d\mathbf{b}_3}{dt} \cdot \mathbf{b}_1 \right) + \mathbf{b}_3 \left(\frac{{}^A d\mathbf{b}_1}{dt} \cdot \mathbf{b}_2 \right) \right] \times \mathbf{b}_1$$

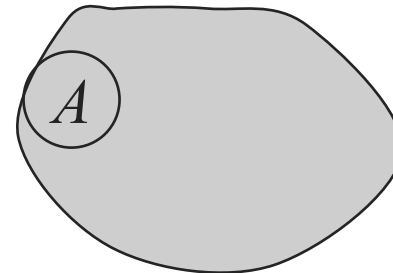
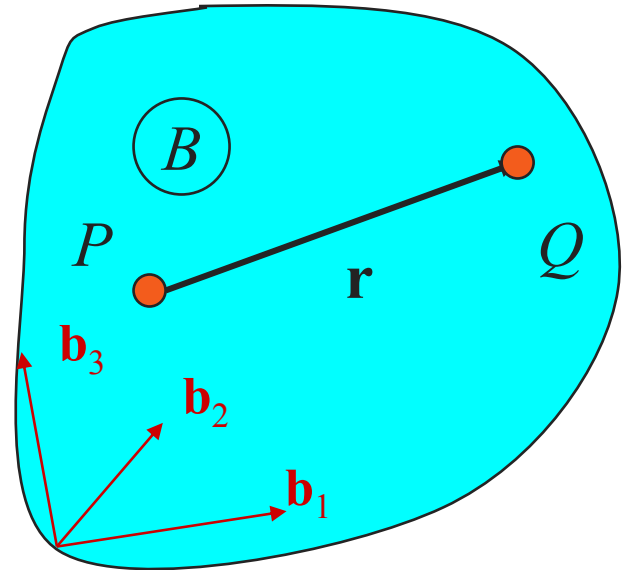
$$\frac{{}^A d\mathbf{b}_1}{dt} = \left(\frac{{}^A d\mathbf{b}_1}{dt} \cdot \mathbf{b}_2 \right) \mathbf{b}_2 - \left(\frac{{}^A d\mathbf{b}_3}{dt} \cdot \mathbf{b}_1 \right) \mathbf{b}_3$$

Important Result 1

$$\frac{{}^A d\mathbf{b}_i}{dt} = {}^A\omega^B \times \mathbf{b}_i$$

Important Result 2

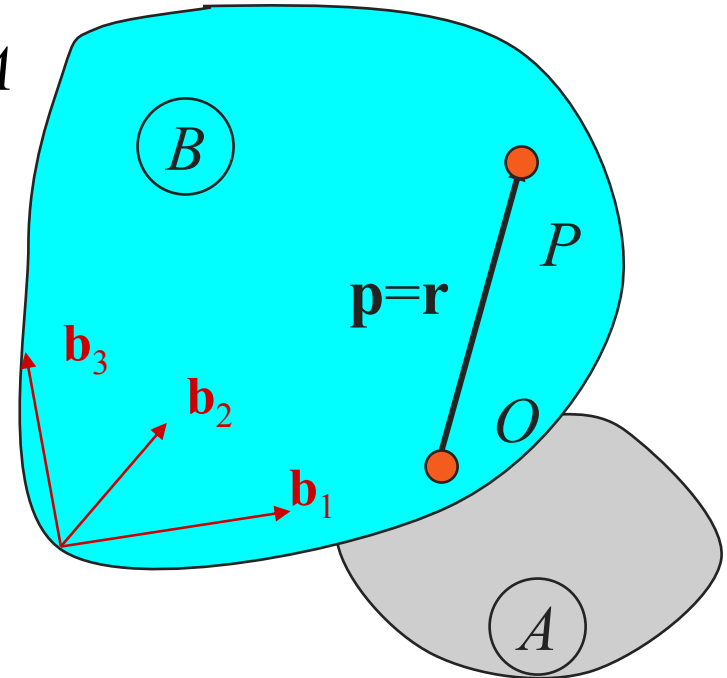
$$\begin{aligned} \frac{{}^A d\mathbf{r}}{dt} &= r_1 \frac{{}^A d\mathbf{b}_1}{dt} + r_2 \frac{{}^A d\mathbf{b}_2}{dt} + r_3 \frac{{}^A d\mathbf{b}_3}{dt} \\ &= r_1 {}^A\omega^B \times \mathbf{b}_1 + r_2 {}^A\omega^B \times \mathbf{b}_2 + r_3 {}^A\omega^B \times \mathbf{b}_3 \\ &= {}^A\omega^B \times \mathbf{r} \end{aligned}$$



Velocity of P (attached to B) in A when A and B have a common point O

Choose \mathbf{p} to be a position vector of P in A

$${}^A \mathbf{v}^P = \frac{{}^A d\mathbf{p}}{dt} = {}^A \boldsymbol{\omega}^B \times \mathbf{p}$$



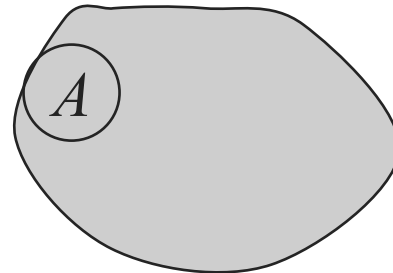
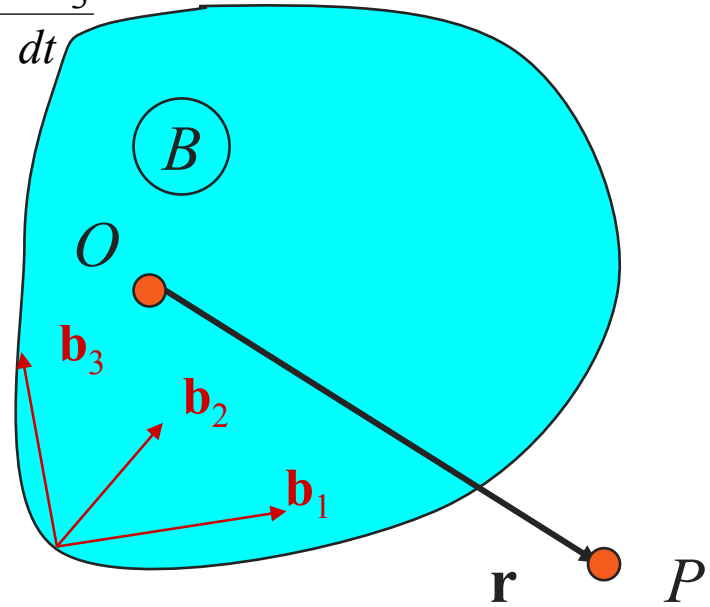
Differentiation of vectors

2. Vector not fixed to B

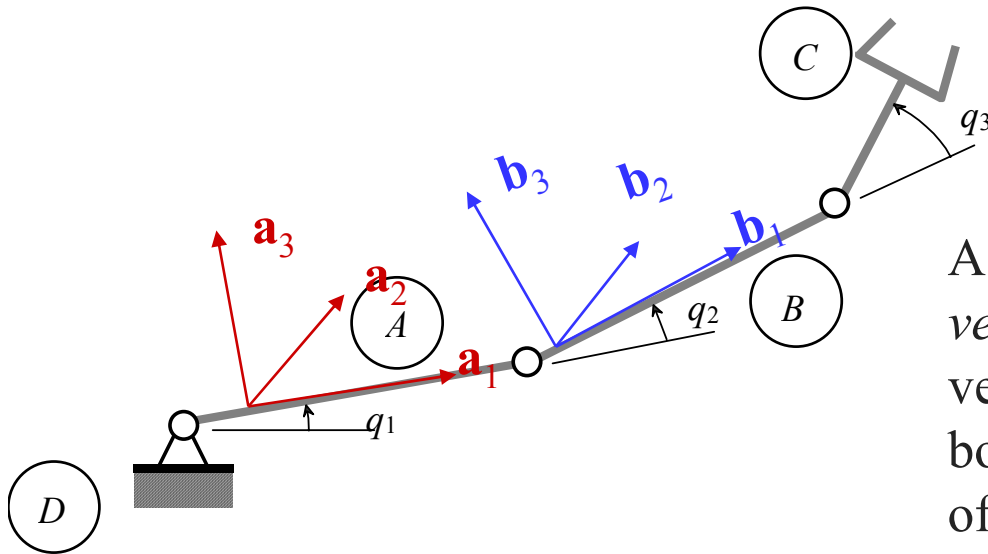
$$\begin{aligned} \frac{{}^A d\mathbf{r}}{dt} &= \frac{dr_1}{dt} \mathbf{b}_1 + \frac{dr_2}{dt} \mathbf{b}_2 + \frac{dr_3}{dt} \mathbf{b}_3 + r_1 \frac{{}^A d\mathbf{b}_1}{dt} + r_2 \frac{{}^A d\mathbf{b}_2}{dt} + r_3 \frac{{}^A d\mathbf{b}_3}{dt} \\ &= \frac{{}^B d\mathbf{r}}{dt} + r_1 {}^A \omega^B \times \mathbf{b}_1 + r_2 {}^A \omega^B \times \mathbf{b}_2 + r_3 {}^A \omega^B \times \mathbf{b}_3 \\ &= \frac{{}^B d\mathbf{r}}{dt} + {}^A \omega^B \times \mathbf{r} \end{aligned}$$

$$\frac{{}^A d\mathbf{r}}{dt} = \frac{{}^B d\mathbf{r}}{dt} + {}^A \omega^B \times \mathbf{r}$$

\mathbf{r} can be *any* vector



Simple Angular Velocity



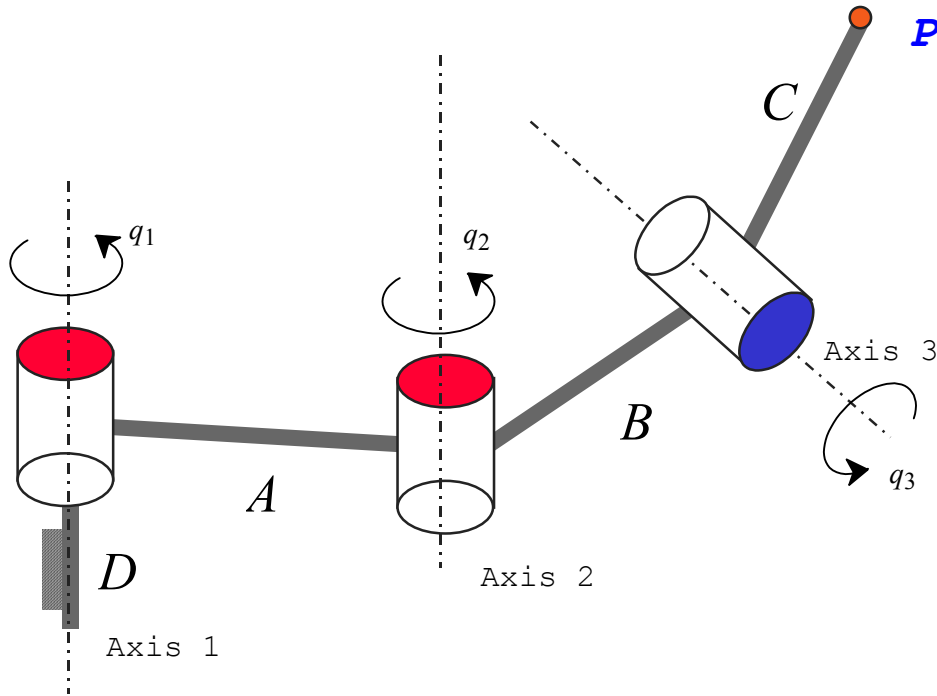
A rigid body B has a *simple angular velocity* in A , when there exists a unit vector \mathbf{k} whose orientation (as seen) in both A and in B is constant (independent of time).

Angular velocity of B in A

- is along \mathbf{a}_2 as seen in A
- is along \mathbf{b}_2 as seen in B

In each frame, the angular velocity has a constant direction (magnitude may change)

Simple Angular Velocity



${}^D\omega^A$, ${}^A\omega^B$ and ${}^C\omega^B$ are simple angular velocities.

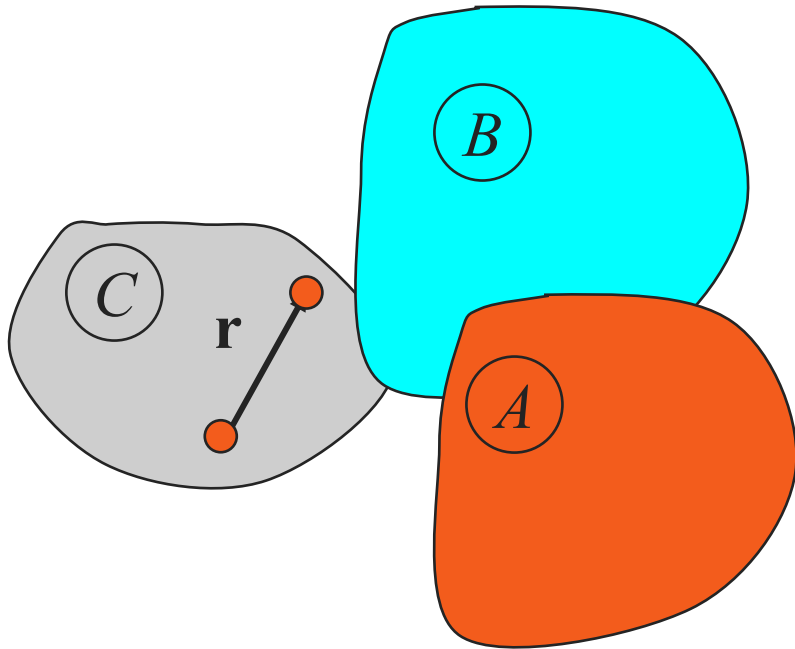
How about ${}^D\omega^C$?

However, ${}^D\omega^C$ is not a simple angular velocity. The motion of C relative to D is such that there is no vector fixed in D that also remains fixed in C.

Addition Theorem for Angular Velocities

Let A , B , and C be three rigid bodies. The addition theorem for angular velocities states:

$${}^A\omega^C = {}^A\omega^B + {}^B\omega^C$$



Proof

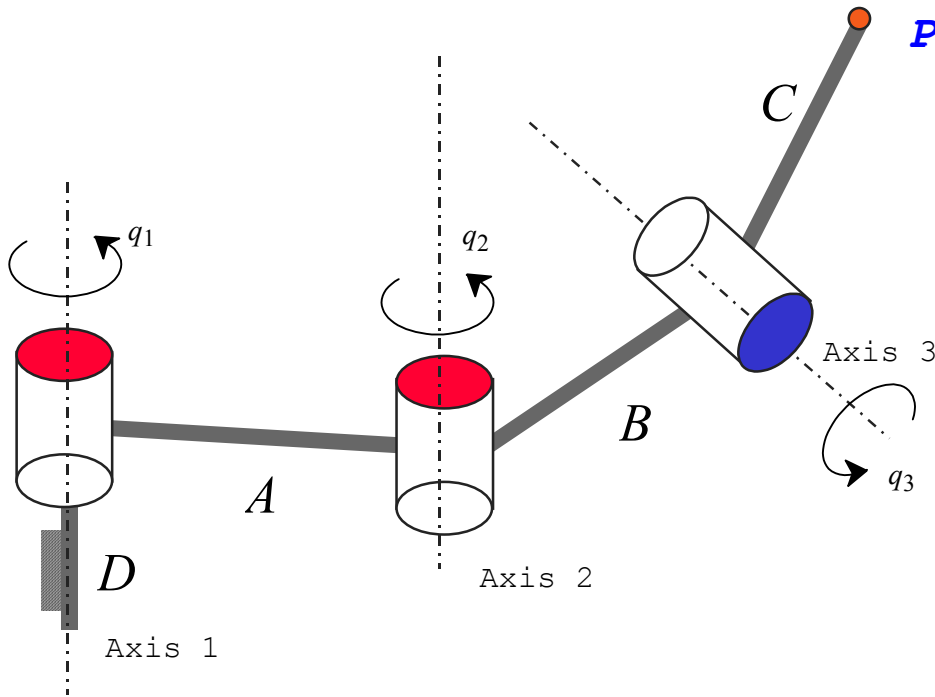
Let \mathbf{r} be fixed to C .

$$\begin{aligned} \frac{{}^A d\mathbf{r}}{dt} &= \frac{{}^B d\mathbf{r}}{dt} + {}^A\omega^B \times \mathbf{r} \\ &= \frac{{}^C d\mathbf{r}}{dt} + {}^B\omega^C \times \mathbf{r} + {}^A\omega^B \times \mathbf{r} \\ &= \frac{{}^C d\mathbf{r}}{dt} + ({}^B\omega^C + {}^A\omega^B) \times \mathbf{r} \\ &= ({}^B\omega^C + {}^A\omega^B) \times \mathbf{r} \end{aligned}$$

And,

$$\frac{{}^A d\mathbf{r}}{dt} = {}^A\omega^C \times \mathbf{r}$$

Angular velocities can be found by adding up “simple” angular velocities



${}^D\omega^C$ is not a simple angular velocity. The motion of C relative to D is such that there is no vector fixed in D that also remains fixed in C.

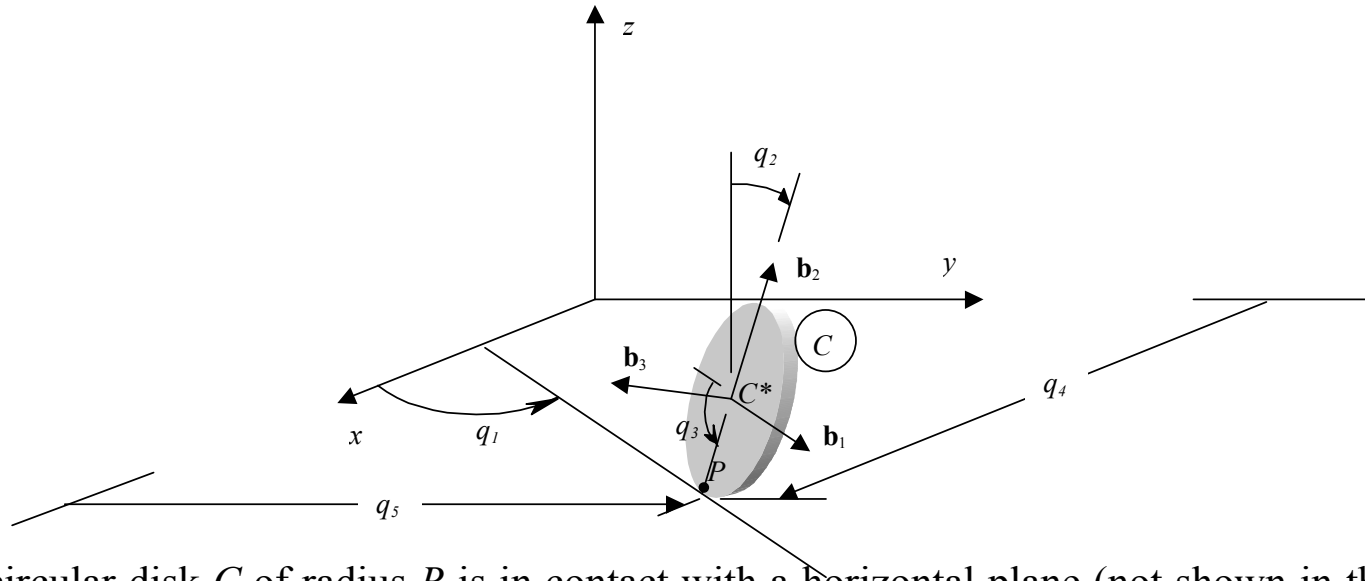
But,

$${}^D\omega^C = {}^D\omega^A + {}^A\omega^B + {}^B\omega^C$$

${}^D\omega^A$, ${}^A\omega^B$ and ${}^B\omega^C$ are simple angular velocities.

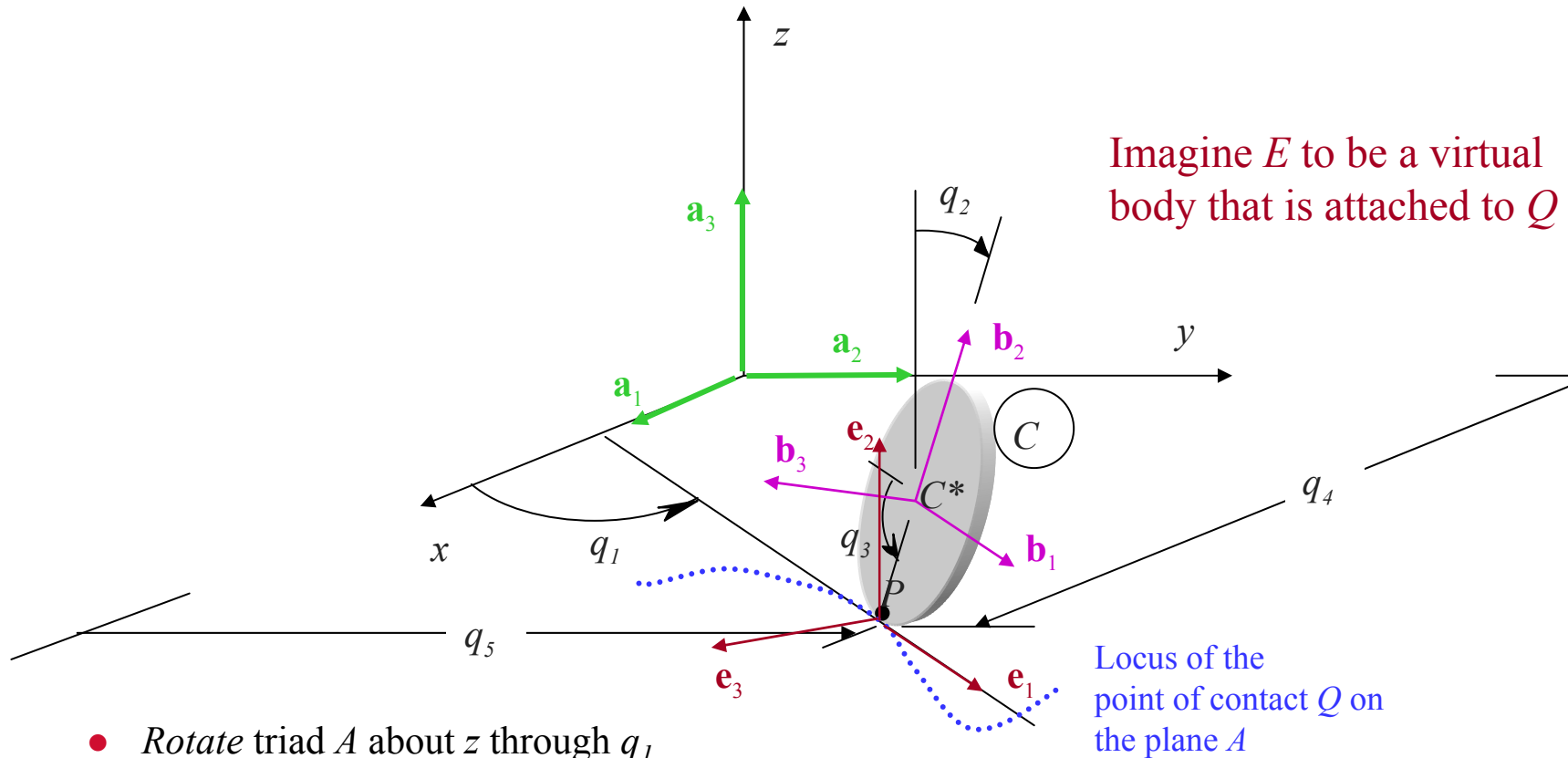
Example

The rolling (and sliding) disk on a horizontal plane



A circular disk C of radius R is in contact with a horizontal plane (not shown in the figure) at the point P . The point P is attached to the disk. The plane is the x - y plane. It is rigidly attached to the earth. The standard reference triad \mathbf{b}_i is chosen so that \mathbf{b}_1 is along the direction of progression of the disk (parallel to the tangent to the disk at P), \mathbf{b}_2 is parallel to the plane of the disk, and \mathbf{b}_3 is normal to the disk. Note that this triad is *not* fixed to the disk. Call the earth-fixed reference frame A and choose the standard reference triad \mathbf{a}_x , \mathbf{a}_y , and \mathbf{a}_z in an obvious fashion along the x , y , and z axes shown in the figure.

Reference Triads



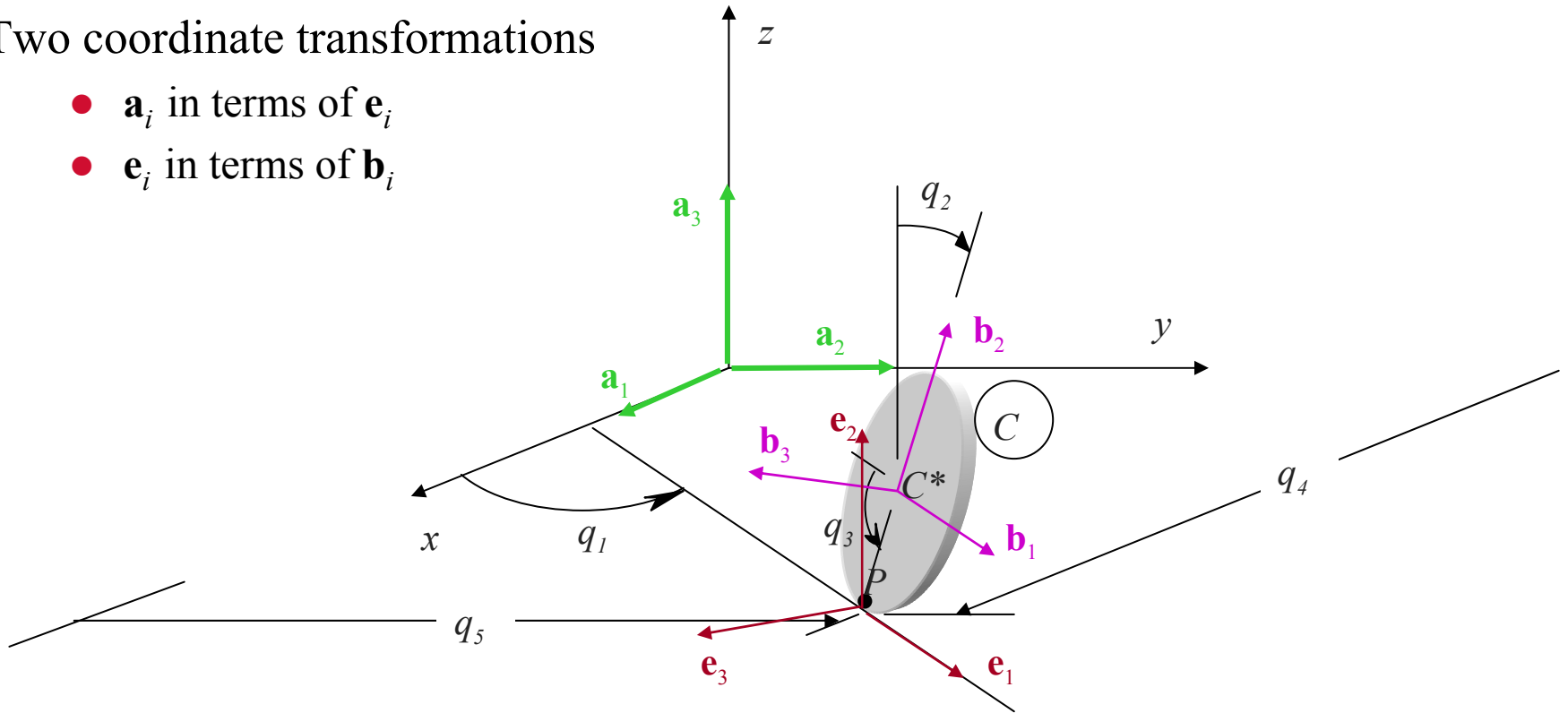
- Rotate triad A about z through q_1 followed by rotation about x by 90 deg to get E
- Rotate triad E about $-x$ through q_2 to get B
- Rotate triad B about z through q_3 to get C (not shown)

Imagine B to be a virtual body that is attached to C^*

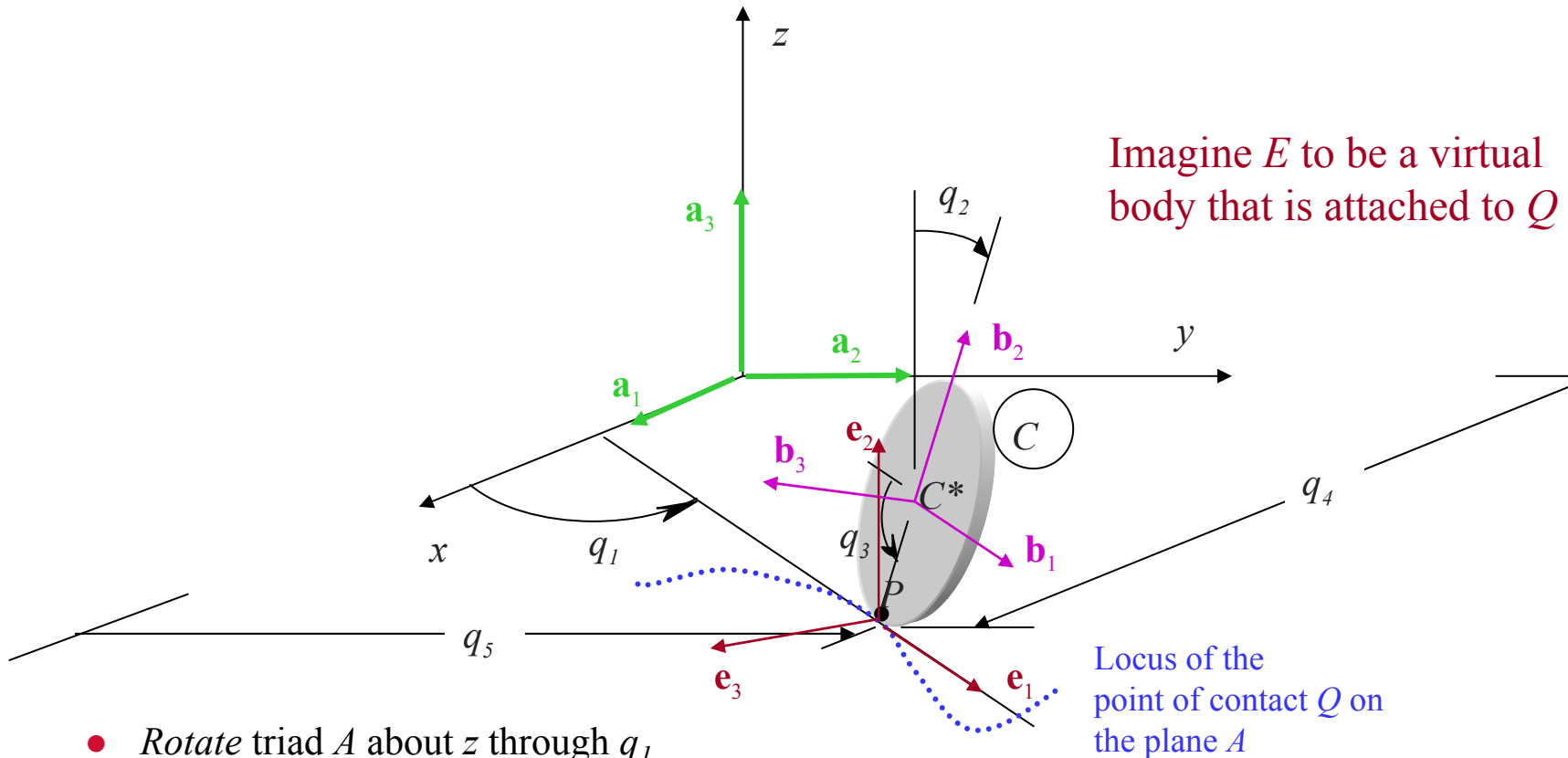
Transformations

Two coordinate transformations

- \mathbf{a}_i in terms of \mathbf{e}_i
- \mathbf{e}_i in terms of \mathbf{b}_i



Reference Triads



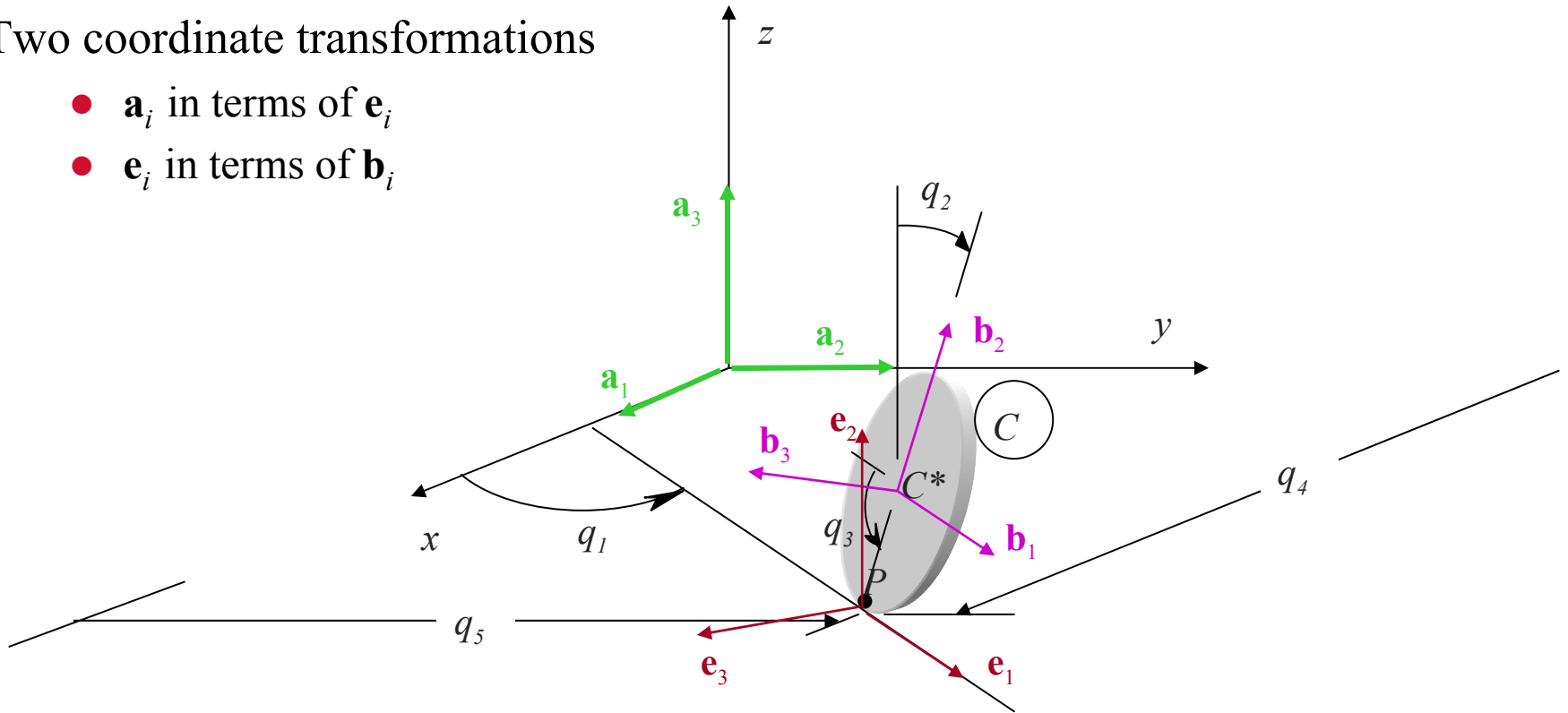
- Rotate triad A about z through q_1 followed by rotation about x by 90 deg to get E
- Rotate triad E about $-x$ through q_2 to get B
- Rotate triad B about z through q_3 to get C (not shown)

Imagine B to be a virtual body that is attached to C^*

Transformations

Two coordinate transformations

- \mathbf{a}_i in terms of \mathbf{e}_i
- \mathbf{e}_i in terms of \mathbf{b}_i



Angular Velocity: Components

$${}^A\boldsymbol{\omega}^C = u_1 \mathbf{b}_1 + u_2 \mathbf{b}_2 + u_3 \mathbf{b}_3$$

- u_i are the components of the angular velocity of the disk with respect to the reference triad B

$$\begin{bmatrix} u_1 \\ u_2 \\ u_3 \\ u_4 \\ u_5 \end{bmatrix} = \mathbf{X} \begin{bmatrix} \dot{q}_1 \\ \dot{q}_2 \\ \dot{q}_3 \\ \dot{q}_4 \\ \dot{q}_5 \end{bmatrix}$$

$${}^A\boldsymbol{\omega}^C = u_x \mathbf{a}_x + u_y \mathbf{a}_y + u_z \mathbf{a}_z$$

- u_α are the components of the angular velocity of the disk with respect to the reference triad A

$$\begin{bmatrix} \dot{q}_1 \\ \dot{q}_2 \\ \dot{q}_3 \\ \dot{q}_4 \\ \dot{q}_5 \end{bmatrix} = \mathbf{Y} \begin{bmatrix} u_1 \\ u_2 \\ u_3 \\ u_4 \\ u_5 \end{bmatrix}$$

Angular Acceleration

The *angular acceleration of B in A*, denoted by ${}^A\alpha^B$, is defined as the first time-derivative in A of the angular velocity of B in A :

$${}^A\alpha^B = \frac{{}^A d}{dt} ({}^A\omega^B)$$

Addition theorem for angular accelerations?