

## ESE 531: Digital Signal Processing

Lec 13: February 23st, 2017  
Frequency Response of LTI Systems

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Adapted from M. Lustig, EECS Berkeley



## Lecture Outline

- Frequency Response of LTI Systems
  - Magnitude Response
    - Simple Filters
  - Phase Response
    - Group Delay
  - Example: Zero on Real Axis

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## Frequency Response of LTI System

- LTI Systems are uniquely determined by their impulse response
$$y[n] = \sum_{k=-\infty}^{\infty} x[k] h[n-k] = x[k] * h[k]$$
- We can write the input-output relation also in the z-domain
$$Y(z) = H(z)X(z)$$
- Or we can define an LTI system with its frequency response
$$Y(e^{j\omega}) = H(e^{j\omega})X(e^{j\omega})$$
- $H(e^{j\omega})$  defines magnitude and phase change at each frequency

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## Frequency Response of LTI System

- $$Y(e^{j\omega}) = H(e^{j\omega})X(e^{j\omega})$$
- We can define a magnitude response
$$|Y(e^{j\omega})| = |H(e^{j\omega})||X(e^{j\omega})|$$
  - And a phase response
$$\angle Y(e^{j\omega}) = \angle H(e^{j\omega}) + \angle X(e^{j\omega})$$

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## Phase Response

- Limit the range of the phase response

$$-\pi < \text{ARG}[H(e^{j\omega})] \leq \pi.$$

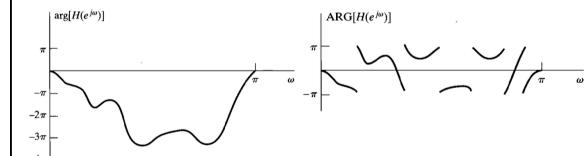
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## Group Delay

- General phase response at a given frequency can be characterized with group delay, which is related to phase

$$\text{grd}[H(e^{j\omega})] = -\frac{d}{d\omega}\{\arg[H(e^{j\omega})]\}$$

- More later...

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## Linear Difference Equations

$$\sum_{k=0}^N a_k y[n-k] = \sum_{k=0}^M b_k x[n-k]$$

Example:  $y[n] = x[n] + 0.1y[n-1]$

$$H(z) = \frac{b_0 + b_1 z^{-1} + \dots + b_M z^{-M}}{a_0 + a_1 z^{-1} + \dots + a_N z^{-N}} = \frac{b_0 \prod_{k=1}^M (1 - c_k z^{-1})}{a_0 \prod_{k=1}^N (1 - d_k z^{-1})}$$

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## Magnitude Response

Magnitude of products is product of magnitudes

$$|H(e^{j\omega})| = \left| \frac{b_0}{a_0} \right| \cdot \frac{\prod_{k=0}^M |1 - c_k e^{-j\omega}|}{\prod_{k=0}^N |1 - d_k e^{-j\omega}|}$$

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## Magnitude Response

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Consider one of the poles:

$$|1 - d_k e^{-j\omega}| = |e^{+j\omega} - d_k| = |v_1|$$

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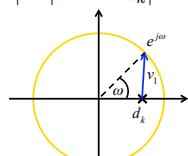
## Magnitude Response

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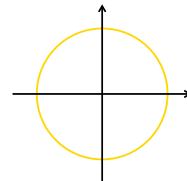
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## Magnitude Response Example

$$H(z) = 0.05 \frac{1 + z^{-1}}{1 - 0.9z^{-1}}$$

$$|H(z)| = 0.05 \frac{|v_2|}{|v_1|}$$



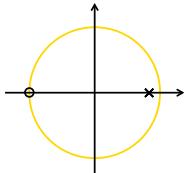
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### Magnitude Response Example

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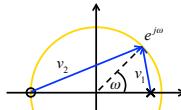
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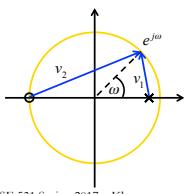
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### Simple Low Pass Filter

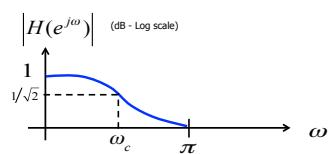
$$H_{LP}(z) = \frac{1 - \alpha}{2} \frac{1 + z^{-1}}{1 - \alpha z^{-1}} \quad |\alpha| < 1$$

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### Simple Low Pass Filter

$$H_{LP}(z) = \frac{1 - \alpha}{2} \frac{1 + z^{-1}}{1 - \alpha z^{-1}} \quad |\alpha| < 1$$



$$\omega_c \text{ is the } 3\text{dB cutoff frequency} \quad \alpha = \frac{1 - \sin(\omega_c)}{\cos(\omega_c)}$$

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### Simple High Pass Filter

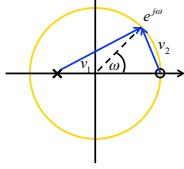
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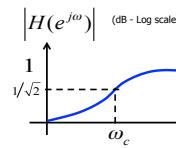


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### Simple High Pass Filter

$$H_{HP}(z) = \frac{1+\alpha}{2} \frac{1-z^{-1}}{1+\alpha z^{-1}} \quad |\alpha| < 1$$



$$w_c \text{ is the } 3\text{dB cutoff frequency} \quad \alpha = \frac{1 - \sin(\omega_c)}{\cos(\omega_c)}$$

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### Simple Band-Stop (Notch) Filter

$$H_{BS}(z) = \frac{1+\alpha}{2} \frac{1-2\beta z^{-1}+z^{-2}}{1-\beta(1+\alpha)z^{-1}+\alpha z^{-2}} \quad |\alpha| < 1 \quad |\beta| < 1$$

Note:  $1-2\beta z^{-1}+z^{-2} = (1-e^{j\omega_0}z^{-1})(1-e^{-j\omega_0}z^{-1})$   
 $\cos(\omega_0) = \beta$

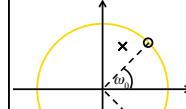
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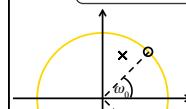
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### Simple Band-Stop (Notch) Filter

$$H_{BS}(z) = \frac{1+\alpha}{2} \frac{1-2\beta z^{-1}+z^{-2}}{1-\beta(1+\alpha)z^{-1}+\alpha z^{-2}} \quad |\alpha| < 1 \quad |\beta| < 1$$

Note:

$$H_{BS}(\mp 1) = \frac{1+\alpha}{2} \frac{2 \pm 2\beta}{(1+\alpha)(1 \pm \beta)} = 1$$



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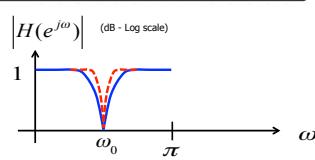
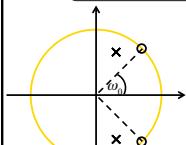
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### Simple Band-Stop (Notch) Filter

$$H_{BS}(z) = \frac{1+\alpha}{2} \frac{1-2\beta z^{-1} + z^{-2}}{1-\beta(1+\alpha)z^{-1} + \alpha z^{-2}} \quad |\alpha| < 1 \quad |\beta| < 1$$

Note: As  $\alpha \rightarrow 1$  poles approach zeros

$$H_{BS}(\mp 1) = \frac{1+\alpha}{2} \frac{2 \pm 2\beta}{(1+\alpha)(1 \pm \beta)} = 1$$



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### Simple Band-Pass Filter

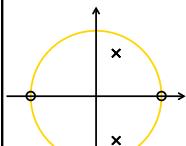
$$H_{BP}(z) = \frac{1-\alpha}{2} \frac{1-z^{-2}}{1-\beta(1+\alpha)z^{-1} + \alpha z^{-2}} \quad |\alpha| < 1 \quad |\beta| < 1$$

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### Simple Band-Pass Filter

$$H_{BP}(z) = \frac{1-\alpha}{2} \frac{1-z^{-2}}{1-\beta(1+\alpha)z^{-1} + \alpha z^{-2}} \quad |\alpha| < 1 \quad |\beta| < 1$$

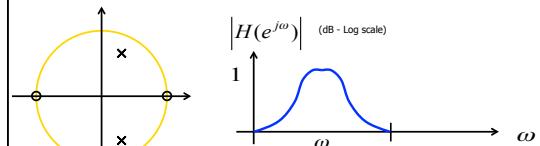


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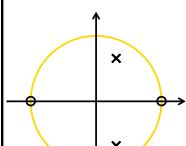


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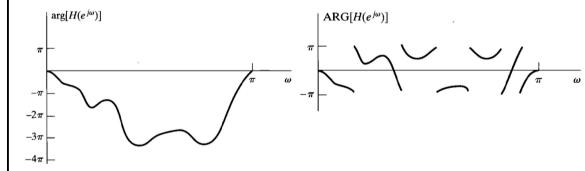
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### Phase Response

- Limit the range of the phase response

$$-\pi < \text{ARG}[H(e^{j\omega})] \leq \pi.$$



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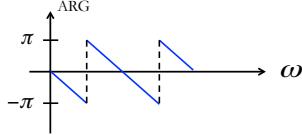
### Phase Response Example

$$H(e^{j\omega}) = e^{j\omega n_d} \leftrightarrow h[n] = \delta[n - n_d]$$

$$|H(e^{j\omega})| = 1$$

$\arg[H(e^{j\omega})] = -\omega n_d$

ARG is the wrapped phase  
arg is the unwrapped phase



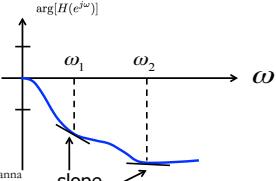
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### Group Delay

- General phase response at a given frequency can be characterized with group delay, which is related to phase

$$\text{grd}[H(e^{j\omega})] = -\frac{d}{d\omega}\{\arg[H(e^{j\omega})]\}$$



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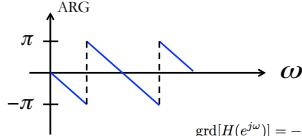
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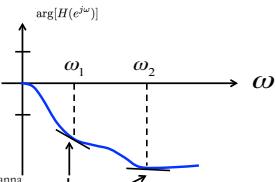
For linear phase system, group delay is  $n_d$

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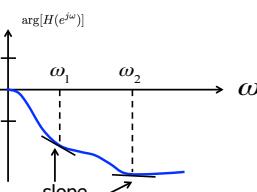
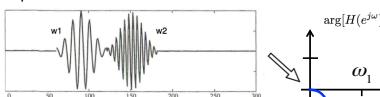
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### Group Delay

$$\text{grd}[H(e^{j\omega})] = -\frac{d}{d\omega}\{\arg[H(e^{j\omega})]\}$$

Input



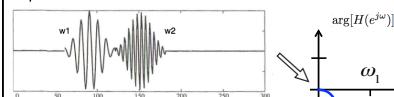
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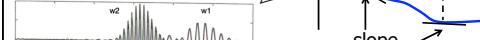
### Group Delay

$$\text{grd}[H(e^{j\omega})] = -\frac{d}{d\omega}\{\arg[H(e^{j\omega})]\}$$

Input



Output



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## Group Delay Math

$$H(z) = \frac{b_0 \prod_{k=1}^M (1 - c_k z^{-1})}{a_0 \prod_{k=1}^N (1 - d_k z^{-1})}$$

$$H(e^{j\omega}) = \frac{b_0 \prod_{k=1}^M (1 - c_k e^{-j\omega})}{a_0 \prod_{k=1}^N (1 - d_k e^{-j\omega})}$$

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## Group Delay Math

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arg of products is sum of args

$$\arg[H(e^{j\omega})] = \sum_{k=1}^M \arg[1 - c_k e^{-j\omega}] - \sum_{k=1}^N \arg[1 - d_k e^{-j\omega}]$$

$$\text{grd}[H(e^{j\omega})] = \sum_{k=1}^M \text{grd}[1 - c_k e^{-j\omega}] - \sum_{k=1}^N \text{grd}[1 - d_k e^{-j\omega}]$$

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## Group Delay Math

$$\text{grd}[H(e^{j\omega})] = \sum_{k=1}^M \text{grd}[1 - c_k e^{-j\omega}] - \sum_{k=1}^N \text{grd}[1 - d_k e^{-j\omega}]$$

Look at each factor:

$$\arg[1 - re^{j\theta} e^{-j\omega}] = \tan^{-1} \left( \frac{r \sin(\omega - \theta)}{1 - r \cos(\omega - \theta)} \right)$$

$$\text{grd}[1 - re^{j\theta} e^{-j\omega}] = \frac{r^2 - r \cos(\omega - \theta)}{|1 - re^{j\theta} e^{-j\omega}|^2}$$

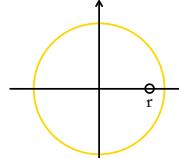
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## Example: Zero on Real Axis

Geometric Interpretation for ( $\theta = 0$ )

$$\arg[1 - re^{-j\omega}]$$



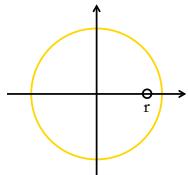
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## Example: Zero on Real Axis

Geometric Interpretation for ( $\theta = 0$ )

$$\arg[1 - re^{-j\omega}] = \arg[(e^{j\omega} - r)e^{-j\omega}] = \underbrace{\arg[e^{j\omega} - r]}_{\varphi} - \underbrace{\arg[e^{j\omega}]}_{\omega}$$



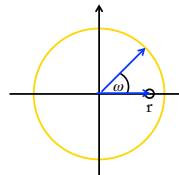
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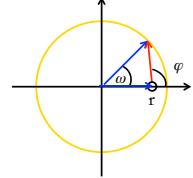
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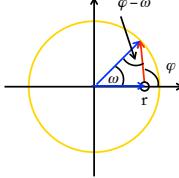
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- Geometric Interpretation for ( $\theta = 0$ )

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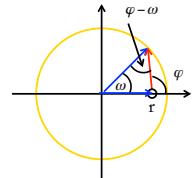
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### Example: Zero on Real Axis

- Geometric Interpretation for ( $\theta = 0$ )

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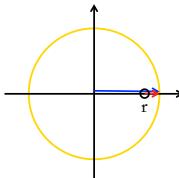
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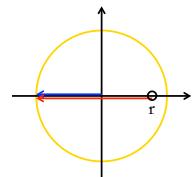
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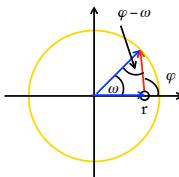
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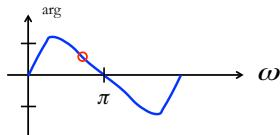
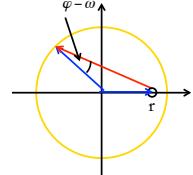
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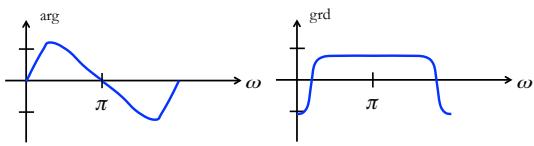
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### Example: Zero on Real Axis

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### Group Delay Math

$$\text{grd}[H(e^{j\omega})] = \sum_{k=1}^M \text{grd}[1 - c_k e^{-j\omega}] - \sum_{k=1}^N \text{grd}[1 - d_k e^{-j\omega}]$$

- Look at each factor:

$$\arg[1 - re^{j\theta} e^{-j\omega}] = \tan^{-1}\left(\frac{r \sin(\omega - \theta)}{1 - r \cos(\omega - \theta)}\right)$$

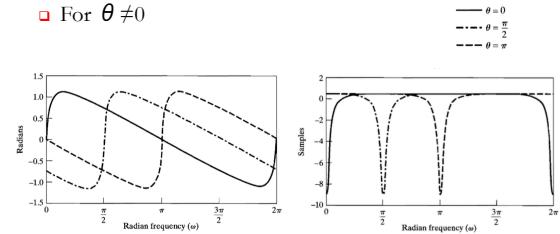
$$\text{grd}[1 - re^{j\theta} e^{-j\omega}] = \frac{r^2 - r \cos(\omega - \theta)}{\left|1 - re^{j\theta} e^{-j\omega}\right|^2}$$

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### Example: Zero on Real Axis

- For  $\theta \neq 0$



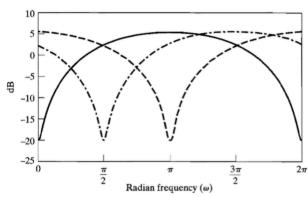
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### Example: Zero on Real Axis

- Magnitude Response

$\theta = 0$   
 $\theta = \frac{\pi}{2}$   
 $\theta = \pi$



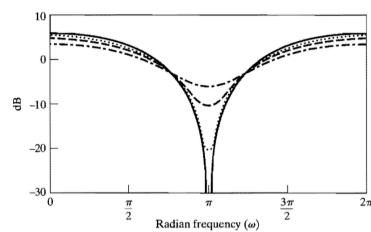
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### Example: Zero on Real Axis

- For  $\theta = \pi$ , how does zero location effect magnitude, phase and group delay?

$r = 0.5$   
 $r = 0.7$   
 $r = 0.9$   
 $r = 1$

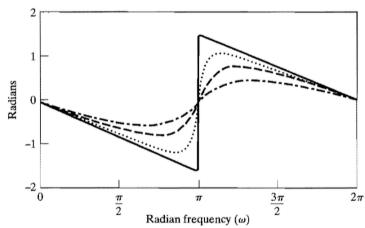


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### Example: Zero on Real Axis

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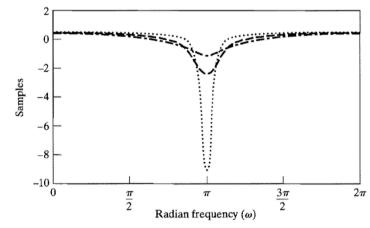


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### Example: Zero on Real Axis

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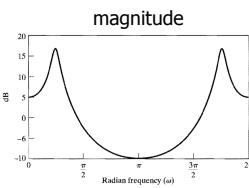


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### 2<sup>nd</sup> Order IIR with Complex Poles

$$H(z) = \frac{1}{(1 - re^{j\theta}z^{-1})(1 - re^{-j\theta}z^{-1})}$$

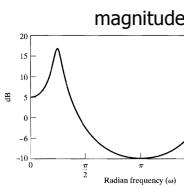


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### Big Ideas

- Frequency Response of LTI Systems
  - Magnitude Response
    - Simple Filters
  - Phase Response
    - Group Delay
  - Example: Zero on Real Axis

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### Admin

- HW 5
  - Due Friday 3/3
- Homework solutions to be posted soon

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