

ESE 531: Digital Signal Processing

Lec 16: March 21, 2019
Design of IIR Filters



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Linear Filter Design

- Used to be an art
 - Now, lots of tools to design optimal filters
- For DSP there are two common classes
 - Infinite impulse response IIR
 - Finite impulse response FIR
- Both classes use finite order of parameters for design

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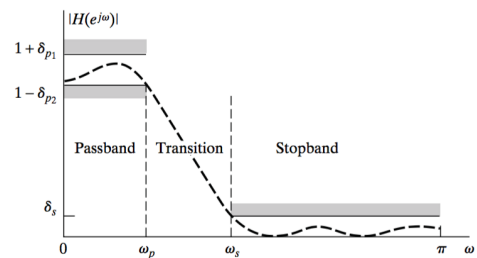
What is a Linear Filter?

- Attenuates certain frequencies
- Passes certain frequencies
- Affects both phase and magnitude
- What does it mean to **design** a filter?
 - Determine the parameters of a transfer function or difference equation that approximates a desired impulse response ($h[n]$) or frequency response ($H(e^{j\omega})$).

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Filter Specifications



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What is a Linear Filter?

- Attenuates certain frequencies
- Passes certain frequencies
- Affects both phase and magnitude
- IIR
 - Mostly non-linear phase response
 - Could be linear over a range of frequencies
- FIR
 - Much easier to control the phase
 - Both non-linear and linear phase

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Today

- IIR Filter Design
 - Impulse Invariance
 - Bilinear Transformation
- Transformation of DT Filters

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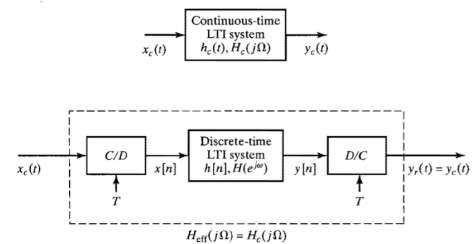
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IIR Filter Design

- Transform continuous-time filter into a discrete-time filter meeting specs
 - Pick suitable transformation from s (Laplace variable) to z (or t to n)
 - Pick suitable analog $H_c(j\omega)$ allowing specs to be met, transform to $H(z)$
- We've seen this before... impulse invariance

Impulse Invariance

- Want to implement continuous-time system in discrete-time



Impulse Invariance

- With $H_c(j\Omega)$ bandlimited, choose

$$H(e^{j\omega}) = H_c(j\frac{\omega}{T}), \quad |\omega| < \pi$$

- With the further requirement that T be chosen such that

$$H_c(j\Omega) = 0, \quad |\Omega| \geq \pi / T$$

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$$h[n] = T h_c(nT)$$

IIR by Impulse Invariance

- If $H_c(j\Omega) = 0$ for $|\Omega| > \pi/T_d$ there is no aliasing and $H(e^{j\omega}) = H_c(j\omega/T_d)$, $|\omega| < \pi$
- To get a particular $H(e^{j\omega})$, find corresponding H_c and T_d for which above is true (within specs)
- Note: T_d is not for aliasing control, used for frequency scaling.

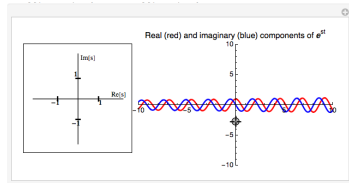
Laplace Transform

- The Laplace transform takes a function of time, t , and transforms it to a function of a complex variable, s .
- Because the transform is invertible, no information is lost and it is reasonable to think of a function $f(t)$ and its Laplace transform $F(s)$ as two views of the same phenomenon.
- Each view has its uses and some features of the phenomenon are easier to understand in one view or the other.

S-Plane

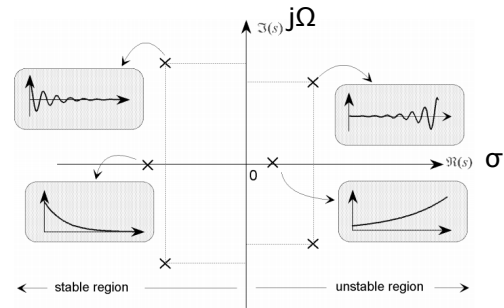
□ $s = \sigma + j\Omega$

□ Wolfram Demo

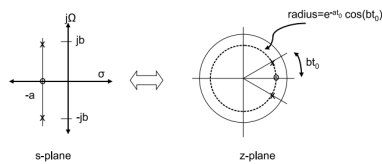


□ <http://pilot.cmsproject.org/content/collection/col10064/latest/module/m10060/latest>

S-plane and stability



S-Plane Mapping to Z-Plane



Example

Example: If $H_c(s) = \frac{A_k}{s - p_k}$

Laplace: $e^{at} \xleftrightarrow{L} \frac{1}{s - a}$

Z-transform: $a^n u[n] \xleftrightarrow{Z} \frac{1}{1 - az^{-1}}$

Example

Example: If $H_c(s) = \frac{A_k}{s - p_k}$ (e.g. one term in PF expansion)

$h_c(t) = A_k e^{p_k t}, t \geq 0; \quad h[n] = T_d A_k e^{p_k T_d n} = T_d A_k (e^{p_k T_d})^n$ Zeros do *not* map the same way; *not* the general mapping of s to z

$\therefore H(z) = T_d A_k \frac{1}{1 - e^{p_k T_d} z^{-1}}$ Pole mapping is $z \leftarrow e^{sT_d}$

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$\therefore H(z) = T_d A_k \frac{1}{1 - e^{p_k T_d} z^{-1}}$ Pole mapping is $z \leftarrow e^{sT_d}$

- Stability, causality, preserved.
- $j\Omega$ axis mapped linearly to unit-circle, with aliasing
- No control of zeros or of phase

Impulse Invariance

- Let,

$$h[n] = T h_c(nT)$$

$$H_c(j\Omega) = 0, \quad |\Omega| \geq \pi/T$$

- If sampling at Nyquist Rate then

$$H(e^{j\omega}) = \sum_{k=-\infty}^{\infty} H_c \left[j \left(\frac{\omega}{T} - \frac{2\pi k}{T} \right) \right]$$

$$H(e^{j\omega}) = H_c \left(j \frac{\omega}{T} \right), \quad |\omega| < \pi$$

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Impulse Invariance

- Sampling the impulse response is equivalent to mapping the s-plane to the z-plane using:
 - $z = e^{sT_d} = r e^{j\omega}$
- The entire Ω axis of the s-plane wraps around the unit circle of the z-plane an infinite number of times

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Impulse Invariance

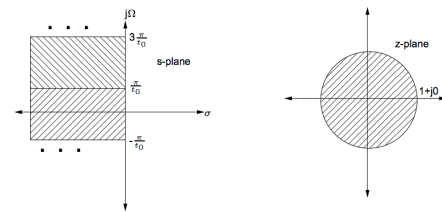
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 - $z = e^{sT_d} = r e^{j\omega}$
- The entire Ω axis of the s-plane wraps around the unit circle of the z-plane an infinite number of times
- The left half s-plane maps to the interior of the unit circle and the right half plane to the exterior

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Impulse Invariance Mapping

Mapping



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Impulse Invariance

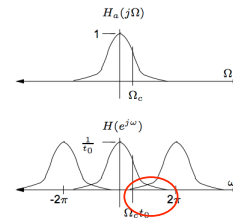
- Sampling the impulse response is equivalent to mapping the s-plane to the z-plane using:
 - $z = e^{sT_d} = r e^{j\omega}$
- The entire Ω axis of the s-plane wraps around the unit circle of the z-plane an infinite number of times
- The left half s-plane maps to the interior of the unit circle and the right half plane to the exterior
- This means stable analog filters (poles in LHP) will transform to stable digital filters (poles inside unit circle)
- This is a many-to-one mapping of strips of the s-plane to regions of the z-plane
 - Not a conformal mapping
 - The poles map according to $z = e^{sT_d}$, but the zeros do not always

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Impulse Invariance

- Limitation of Impulse Invariance: overlap of images of the frequency response. This prevents it from being used for high-pass filter design



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Bilinear Transformation

- The technique uses an algebraic transformation between the variables s and z that maps the entire $j\Omega$ -axis in the s -plane to one revolution of the unit circle in the z -plane.

$$s = \frac{2}{T_d} \left(\frac{1 - z^{-1}}{1 + z^{-1}} \right);$$

$$H(z) = H_c \left(\frac{2}{T_d} \left(\frac{1 - z^{-1}}{1 + z^{-1}} \right) \right).$$

Bilinear Transformation

$$s = \frac{2}{T_d} \left(\frac{1 - z^{-1}}{1 + z^{-1}} \right);$$

- Substituting $s = \sigma + j\Omega$ and $z = e^{j\omega}$

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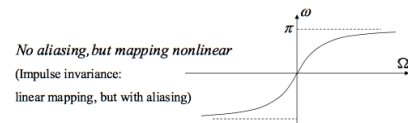
$$s = \frac{2}{T_d} \left(\frac{1 - e^{-j\omega}}{1 + e^{-j\omega}} \right),$$

$$s = \sigma + j\Omega = \frac{2}{T_d} \left[\frac{2e^{-j\omega/2}(j \sin \omega/2)}{2e^{-j\omega/2}(\cos \omega/2)} \right] = \frac{2j}{T_d} \tan(\omega/2).$$

Bilinear Transformation

$$\Omega = \frac{2}{T_d} \tan(\omega/2),$$

$$\omega = 2 \arctan(\Omega T_d/2).$$



Example: Notch Filter

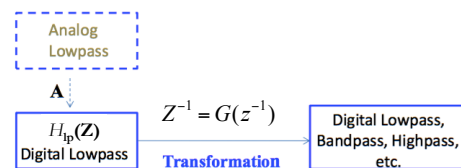
- The continuous time filter with:

$$H_a(s) = \frac{s^2 + \Omega_0^2}{s^2 + Bs + \Omega_0^2}$$

$$\Omega = \frac{2}{T_d} \tan(\omega/2),$$

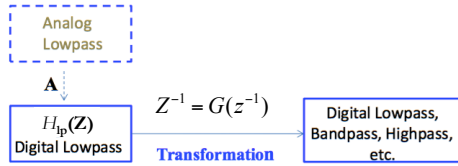
$$\omega = 2 \arctan(\Omega T_d/2).$$

Transformation of DT Filters



- Z – complex variable for the LP filter
- z – complex variable for the transformed filter
- Map Z -plane $\rightarrow$ z -plane with transformation G

Transformation of DT Filters



- Map Z-plane $\rightarrow$ z-plane with transformation G

$$H(z) = H_p(Z) \big|_{Z^{-1}=G(z^{-1})}$$

Example 1:

- Lowpass $\rightarrow$ highpass

- Shift frequency by π

so $\omega \rightarrow \omega - \pi$ (Lowpass to highpass)

$$Z^{-1} = -z^{-1} \text{ or } e^{-j\omega} \rightarrow e^{-j(\omega - \pi)}$$

Example 1:

- Lowpass $\rightarrow$ highpass

- Shift frequency by π

so $\omega \rightarrow \omega - \pi$ (Lowpass to highpass)

$$Z^{-1} = -z^{-1} \text{ or } e^{-j\omega} \rightarrow e^{-j(\omega - \pi)}$$

$$\boxed{y[n] = 0.9y[n-1] + 0.1x[n]} \quad \text{lowpass; pole: } z = 0.9, \quad H(z) = \frac{0.1}{1 - 0.9z^{-1}}$$

$$H(-z) = \frac{0.1}{1 + 0.9z^{-1}} \quad \text{highpass; pole: } z = -0.9 \quad \boxed{y[n] = -0.9y[n-1] + 0.1x[n]}$$

Example 2:

- Lowpass $\rightarrow$ bandpass

$$Z^{-1} = -z^{-2}$$

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- Lowpass $\rightarrow$ bandpass

$$Z^{-1} = -z^{-2} \quad \longrightarrow \quad H_{lp}(z) = \frac{1}{1 - az^{-1}} \quad \longrightarrow \quad H_{bp}(z) = \frac{1}{1 + az^{-2}}$$

Pole at $z=a$ Pole at $z=\pm j\sqrt{a}$

Example 2:

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Pole at $z=a$ Pole at $z=\pm j\sqrt{a}$

- Lowpass $\rightarrow$ bandstop

$$Z^{-1} = z^{-2} \quad \longrightarrow \quad H_{lp}(z) = \frac{1}{1 - az^{-1}} \quad \longrightarrow \quad H_{bs}(z) = \frac{1}{1 - az^{-2}}$$

Pole at $z=\pm\sqrt{a}$

Transformation Constraints on $G(z^{-1})$

- If $H_{lp}(Z)$ is the rational system function of a causal and stable system, we naturally require that the transformed system function $H(z)$ be a rational function and that the system also be causal and stable.
 - $G(Z^{-1})$ must be a rational function of z^{-1}
 - The inside of the unit circle of the Z -plane must map to the inside of the unit circle of the z -plane
 - The unit circle of the Z -plane must map onto the unit circle of the z -plane.

Transformation Constraints on $G(z^{-1})$

- Respective unit circles in both planes

$$Z = e^{j\theta} \text{ and } z = e^{j\omega}$$

Transformation Constraints on $G(z^{-1})$

- Respective unit circles in both planes

$$Z = e^{j\theta} \text{ and } z = e^{j\omega}$$

$$Z^{-1} = G(z^{-1})$$

$$e^{-j\theta} = G(e^{-j\omega})$$

$$e^{-j\theta} = |G(e^{-j\omega})| e^{j\angle G(e^{-j\omega})}$$

Transformation Constraints on $G(z^{-1})$

- Respective unit circles in both planes

$$Z = e^{j\theta} \text{ and } z = e^{j\omega}$$

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$$1 = |G(e^{-j\omega})| \quad -\theta = \angle G(e^{-j\omega})$$

Transformation Constraints on $G(z^{-1})$

- General form that meets all constraints:
 - a_k real and $|a_k| < 1$

$$G(z^{-1}) = \pm \prod_{k=1}^N \frac{z^{-1} - \alpha_k}{1 - \alpha_k^* z^{-1}}$$

General Transformation

- Lowpass $\rightarrow$ lowpass

$$G(z^{-1}) = \frac{z^{-1} - \alpha}{1 - \alpha^* z^{-1}}$$

- Changes passband/stopband edge frequencies

General Transformation

- Lowpass $\rightarrow$ lowpass

$$G(z^{-1}) = \frac{z^{-1} - \alpha}{1 - \alpha z^{-1}}$$

- Changes passband/stopband edge frequencies

From $e^{-j\theta} = \frac{e^{-j\omega} - \alpha}{1 - \alpha e^{-j\omega}}$, get

$$\omega(\theta) = \tan^{-1} \left(\frac{(1 - \alpha^2) \sin(\theta)}{2\alpha + (1 + \alpha^2) \cos(\theta)} \right)$$

General Transformation

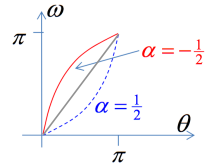
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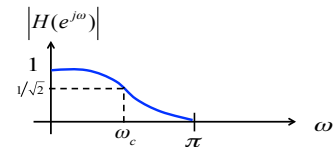
General Transformations

TABLE 7.1 TRANSFORMATIONS FROM A LOWPASS DIGITAL FILTER PROTOTYPE OF CUTOFF FREQUENCY ω_p TO HIGHPASS, BANDPASS, AND BANDSTOP FILTERS

Filter Type	Transformations	Associated Design Formulas
Lowpass	$z^{-1} = \frac{z^{-1} - \alpha}{1 - \alpha z^{-1}}$	$\alpha = \frac{\sin\left(\frac{\omega_p - \omega_c}{2}\right)}{\sin\left(\frac{\omega_p + \omega_c}{2}\right)}$ ω_p = desired cutoff frequency
Highpass	$z^{-1} = -\frac{z^{-1} + \alpha}{1 + \alpha z^{-1}}$	$\alpha = -\frac{\cos\left(\frac{\omega_p + \omega_c}{2}\right)}{\cos\left(\frac{\omega_p - \omega_c}{2}\right)}$ ω_p = desired cutoff frequency
Bandpass	$z^{-1} = \frac{z^{-2} - \frac{2\cos(\omega_c)}{1 + \cos(\omega_p)} z^{-1} + \frac{1 - \cos(\omega_p)}{1 + \cos(\omega_p)}}{\frac{1 - \cos(\omega_p)}{1 + \cos(\omega_p)} z^{-2} - \frac{2\cos(\omega_c)}{1 + \cos(\omega_p)} z^{-1} + 1}$	$k = \cos\left(\frac{\omega_p - \omega_c}{2}\right)$ $\alpha = \frac{\cos\left(\frac{\omega_p + \omega_c}{2}\right)}{\cos\left(\frac{\omega_p - \omega_c}{2}\right)}$ ω_{p1} = desired lower cutoff frequency ω_{p2} = desired upper cutoff frequency
Bandstop	$z^{-1} = \frac{z^{-2} - \frac{2\cos(\omega_c)}{1 - \cos(\omega_p)} z^{-1} + \frac{1 - \cos(\omega_p)}{1 - \cos(\omega_p)}}{\frac{1 - \cos(\omega_p)}{1 - \cos(\omega_p)} z^{-2} - \frac{2\cos(\omega_c)}{1 - \cos(\omega_p)} z^{-1} + 1}$	$k = \cos\left(\frac{\omega_p - \omega_c}{2}\right)$ $\alpha = \frac{\cos\left(\frac{\omega_p + \omega_c}{2}\right)}{\cos\left(\frac{\omega_p - \omega_c}{2}\right)}$ ω_{p1} = desired lower cutoff frequency ω_{p2} = desired upper cutoff frequency

Reminder: Simple Low Pass Filter

$$H_{LP}(z) = \frac{1 - \alpha}{2} \frac{1 + z^{-1}}{1 - \alpha z^{-1}} \quad |\alpha| < 1$$



ω_c is the 3dB cutoff frequency $\alpha = \frac{1 - \sin(\omega_c)}{\cos(\omega_c)}$

Big Idea

- IIR
 - Design from continuous time filters with mapping of s-plane onto z-plane
 - Linear mapping – impulse invariance
 - Non-linear mapping – bilinear transformation
- DT filter transformations
 - Transform z-plane with rational function $G(z^{-1})$
 - Constraints on G for causal/stable systems

Admin

- HW 6
 - Out now
 - Due Sunday 3/24