

LTI Systems

A system 
$$\mathcal{H}$$
 is linear time-invariant (LTI) if it is both linear and time-invariant

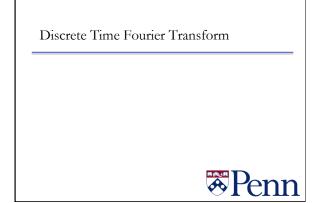
LTI system can be completely characterized by its impulse response

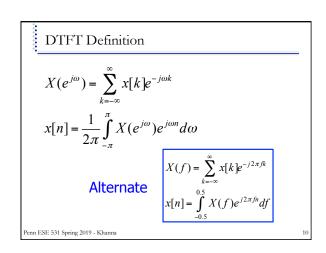
 $\delta \longrightarrow \mathcal{H} \longrightarrow h$ 

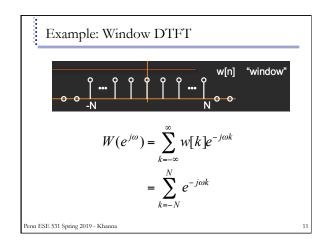
Then the output for an arbitrary input is a sum of weighted, delay impulse responses

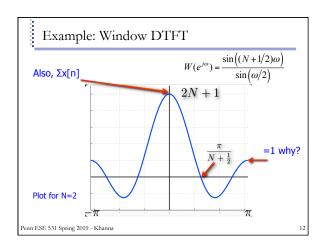
 $x \longrightarrow h \longrightarrow y \qquad y[n] = \sum_{m=-\infty}^{\infty} h[n-m] x[m]$ 
 $y[n] = x[n] * h[n]$ 

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## LTI System Frequency Response

□ Fourier Transform of impulse response

$$x[n]=e^{j\omega n} \longrightarrow LTI System \longrightarrow y[n]=H(e^{j\omega n})e^{j\omega n}$$

$$H(e^{j\omega}) = \sum_{k=-\infty}^{\infty} h[k]e^{-j\omega k}$$

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### z-Transform

- □ The z-transform generalizes the Discrete-Time Fourier Transform (DTFT) for analyzing infinitelength signals and systems
- Very useful for designing and analyzing signal processing systems
- Properties are very similar to the DTFT with a few caveats

$$H(z) = \sum_{n=-\infty}^{\infty} h[n]z^{-n}$$

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Region of Convergence (ROC)

Given a time signal x[n], the **region of convergence** (ROC) of its z-transform X(z) is the set of  $z\in\mathbb{C}$  such that X(z) converges, that is, the set of  $z\in\mathbb{C}$  such that x[n]  $z^{-n}$  is absolutely summable

$$\sum_{n=-\infty}^{\infty} |x[n] \, z^{-n}| \; < \; \infty$$

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Inverse z-Transform

- Ways to avoid it:
  - Inspection (known transforms)
  - Properties of the z-transform
  - Partial fraction expansion

$$X(z) = \frac{b_0}{a_0} \prod_{k=1}^{M} (1 - c_k z^{-1}) = \sum_{k=1}^{N} \frac{A_k}{1 - d_k z^{-1}}$$

Power series expansion

$$X(z) = \sum_{n=-\infty}^{\infty} x[n]z^{-n}$$

 $= \cdots + x[-2]z^{2} + x[-1]z + x[0] + x[1]z^{-1} + x[2]z^{-2} + \cdots$ 

Difference Equation to z-Transform

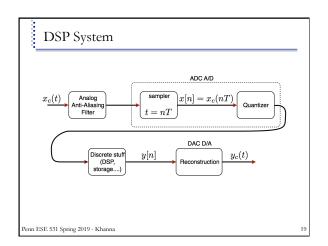
$$\sum_{k=0}^{N} a_k y[n-k] = \sum_{m=0}^{M} b_m x[n-m]$$

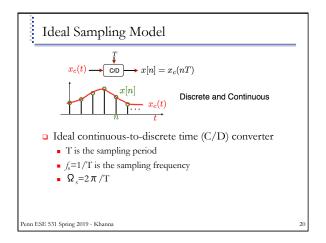
$$H(z) = \frac{\sum_{m=0}^{M} (b_k) z^{-k}}{\sum_{k=0}^{N} (a_k) z^{-k}}$$

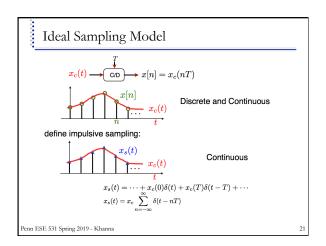
- Difference equations of this form behave as causal LTI systems
  - when the input is zero prior to n=0
  - Initial rest equations are imposed prior to the time when input becomes nonzero
    - i.e y[-N]=y[-N+1]=...=y[-1]=0

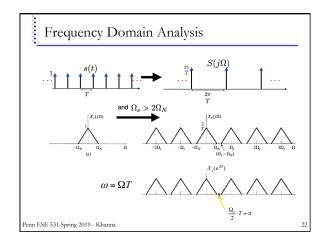
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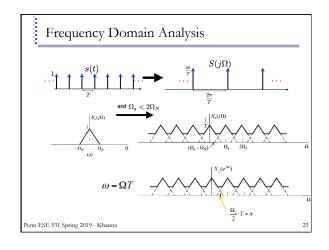
Sampling and Reconstruction

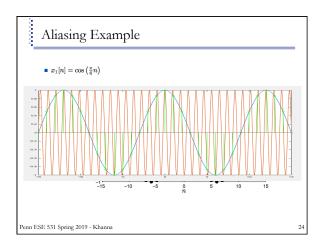










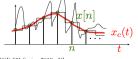


## Reconstruction of Bandlimited Signals

f u Nyquist Sampling Theorem: Suppose  $x_c(t)$  is bandlimited. I.e.

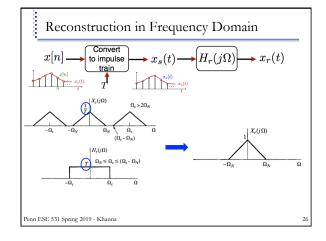
$$X_c(j\Omega) = 0 \ \forall \ |\Omega| \ge \Omega_N$$

- □ If  $\Omega_s \ge 2\Omega_N$ , then  $x_c(t)$  can be uniquely determined from its samples  $x[n] = x_c(nT)$
- □ Bandlimitedness is the key to uniqueness

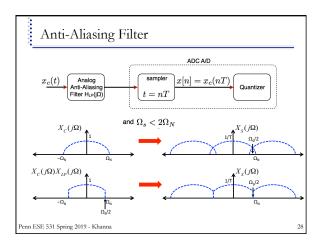


Mulitiple signals go through the samples, but only one is bandlimited within our sampling band

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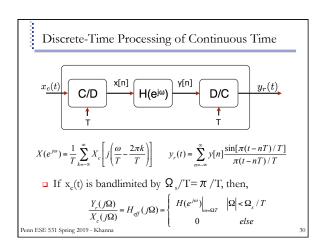


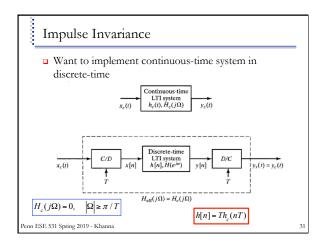
# Reconstruction in Time Domain $x_r(t) = x_s(t) * h_r(t) = \left(\sum_n x[n]\delta(t-nT)\right) * h_r(t)$ $= \sum_n x[n]h_r(t-nT)$ $= \sum_n x[n]h_r(t-nT)$ The sum of "sincs" gives $x_r(t) \Rightarrow$ unique signal that is bandlimited by sampling bandwidth

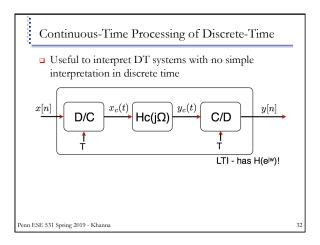


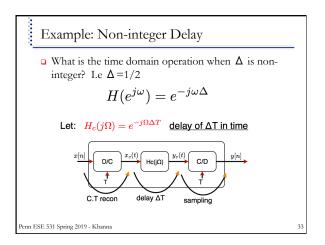
# DT and CT processing

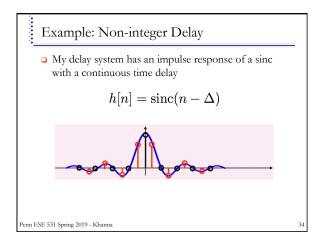


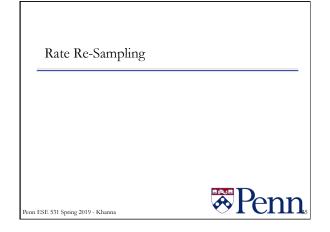


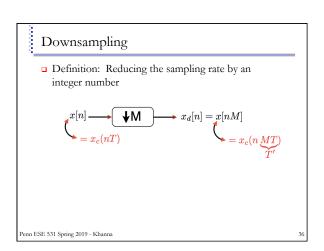


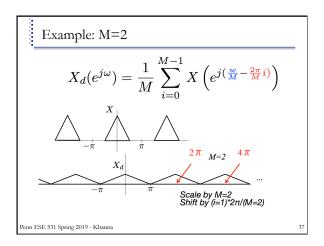


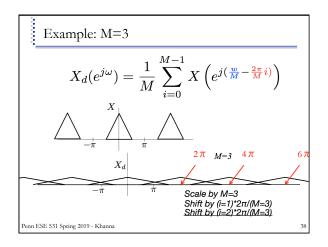


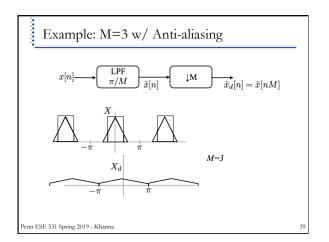


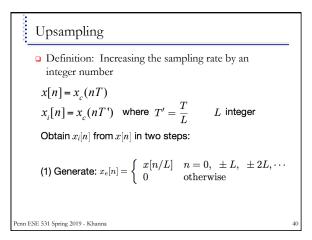


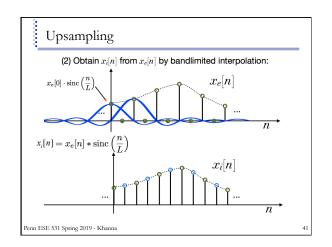


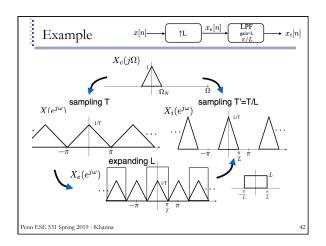


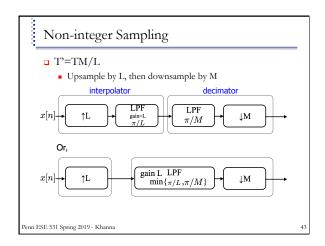


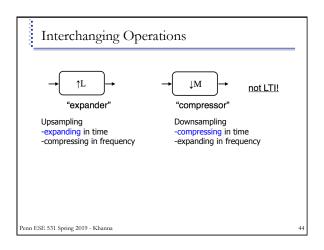


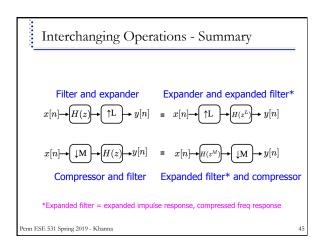


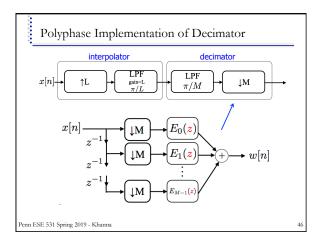


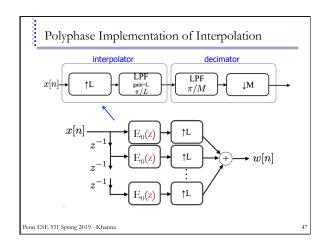


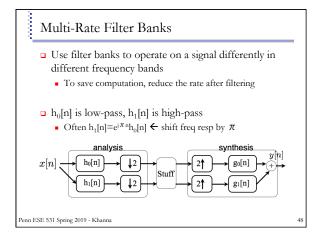


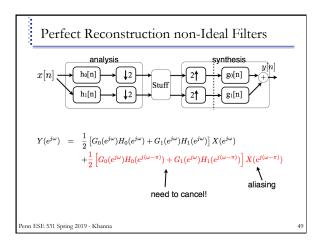


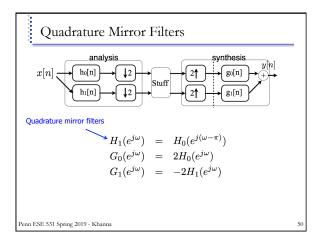












Frequency Response of Systems

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Frequency Response of LTI System

$$Y(e^{j\omega}) = H(e^{j\omega})X(e^{j\omega})$$

□ We can define a magnitude response

$$|Y(e^{j\omega})| = |H(e^{j\omega})||X(e^{j\omega})|$$

□ And a phase response

$$\angle Y(e^{j\omega}) = \angle H(e^{j\omega}) + \angle X(e^{j\omega})$$

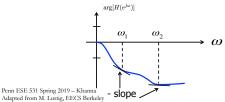
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## Group Delay

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 General phase response at a given frequency can be characterized with group delay, which is related to phase

$$\operatorname{grd}[H(e^{j\omega})] = -\frac{d}{d\omega} \{ \operatorname{arg}[H(e^{j\omega})] \}$$



LTI System

$$\sum_{k=0}^{N} a_k y[n-k] = \sum_{k=0}^{M} b_k x[n-k]$$

Example: y[n] = x[n] + 0.1y[n-1]

Stable and causal f all poles inside unit circle

$$H(z) = \frac{b_0 + b_1 z^{-1} + \ldots + b_M z^{-M}}{a_0 + a_1 z^{-1} + \ldots + a_N z^{-N}} = \frac{b_0}{a_0} \frac{\prod_{k=1}^M (1 - c_k z^{-1})}{\prod_{k=1}^N (1 - d_k z^{-1})}$$

- □ Transfer function is not unique without ROC
  - If diff. eq represents LTI and causal system, ROC is region outside all singularities
  - If diff. eq represents LTI and stable system, ROC includes unit circle in z-plane

### General All-Pass Filter

d<sub>k</sub>=real pole, e<sub>k</sub>=complex poles paired w/ conjugate, e<sub>k</sub>\*

$$H_{\mathrm{ap}}(z) = A \prod_{k=1}^{M_r} \frac{z^{-1} - d_k}{1 - d_k z^{-1}} \prod_{k=1}^{M_c} \frac{(z^{-1} - e_k^*)(z^{-1} - e_k)}{(1 - e_k z^{-1})(1 - e_k^* z^{-1})}$$

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# Minimum-Phase Systems Definition: A stable and causal system H(z) (i.e. poles inside unit circle) whose inverse 1/H(z) is also stable and causal (i.e. zeros inside unit circle) All poles and zeros inside unit circle 1/H(z) Yenn ESE 531 Spring 2019 - Khanna

## Min-Phase Decomposition Purpose

□ Have some distortion that we want to compensate for: G(z)

 $\begin{array}{c|c} G(z) \\ \hline & Distorting \\ s_I[n] & H_d(z) \\ \hline \\ & H_d(z) \\ \hline \end{array} \begin{array}{c|c} Compensating \\ system \\ H_c(z) \\ \hline \\ & S_c[n] \\ \hline \end{array}$ 

- $\Box$  If  $H_d(z)$  is min phase, easy:
  - $H_c(z)=1/H_d(z)$   $\leftarrow$  also stable and causal
- $\Box$  Else, decompose  $H_d(z)=H_{d,min}(z) H_{d,ap}(z)$ 
  - $H_c(z)=1/H_{d,min}(z) \rightarrow H_d(z)H_c(z)=H_{d,ap}(z)$ 
    - Compensate for magnitude distortion

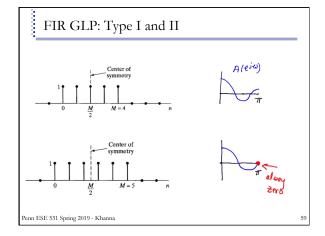
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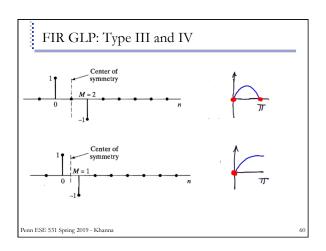
# Generalized Linear Phase

□ An LTI system has generalized linear phase if frequency response  $H(e^{j\omega})$  can be expressed as:

$$H(e^{j\omega}) = A(\omega)e^{-j\omega\alpha+j\beta}, \ |\omega| < \pi$$

- f u What is the group delay?





Zeros of GLP System

□ FIR GLP System Function

$$H(z) = \sum_{n=0}^{M} h[n] z^{-n}$$

Real system  $\rightarrow$  zeros occur in conjugate-reciprocal groups of 4

$$(1-re^{j\theta}z^{-1})(1-re^{-j\theta}z^{-1})(1-r^{-1}e^{j\theta}z^{-1})(1-r^{-1}e^{-j\theta}z^{-1})$$

☐ If zero is on unit circle (r=1)

$$(1-e^{j\theta}z^{-1})(1-e^{-j\theta}z^{-1}).$$

 $\Box$  If zero is real and not on unit circle ( $\theta = 0$ )

$$(1 \pm rz^{-1})(1 \pm r^{-1}z^{-1}).$$

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FIR Filter Design

FIR Design by Windowing

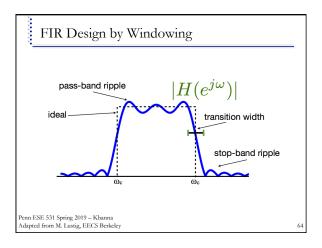
 $\Box$  Given desired frequency response,  $H_d(e^{j\omega})$ , find an impulse response

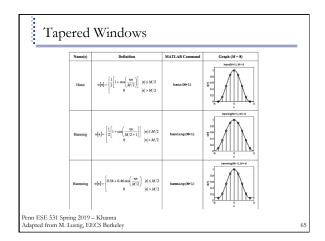
$$h_d[n] = \frac{1}{2\pi} \int_{-\pi}^{\pi} H_d(\underbrace{e^{j\omega})} e^{j\omega n} d\omega \hspace{0.2in} \xrightarrow{\hspace{0.2in} \text{ideal}}$$

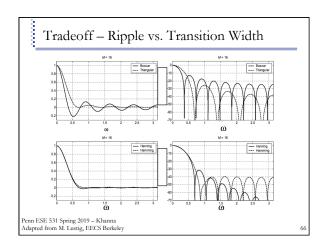
Obtain the Mth order causal FIR filter by truncating/windowing it

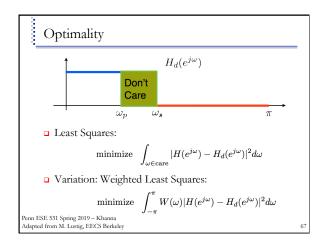
$$h[n] = \left\{ \begin{array}{ll} h_d[n]w[n] & 0 \leq n \leq M \\ 0 & \text{otherwise} \end{array} \right\}$$

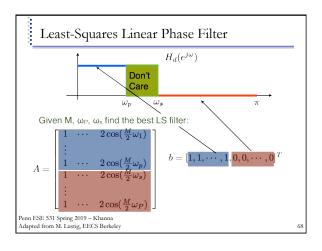
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Min-Max Ripple Design

Recall,  $\tilde{H}(e^{j\omega})$  is symmetric and real
Given  $\omega_p$ ,  $\omega_s$ , M, find  $\delta$ ,  $\tilde{h}_+$   $\frac{1+\delta}{1-\delta}$ minimize  $\delta$ Subject to:  $1-\delta \leq \tilde{H}(e^{j\omega_k}) \leq 1+\delta \quad 0 \leq \omega_k \leq \omega_p$   $-\delta \leq \tilde{H}(e^{j\omega_k}) \leq \delta \quad \omega_s \leq \omega_k \leq \pi$   $\delta > 0$ Formulation is a linear program with solution  $\delta$ ,  $\tilde{h}_+$ A well studied class of problems

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IIR Filter Design

IIR Filter Design
 □ Transform continuous-time filter into a discrete-time filter meeting specs
 ■ Pick suitable transformation from s (Laplace variable) to z (or t to n)
 ■ Pick suitable analog H<sub>s</sub>(s) allowing specs to be met, transform to H(z)
 □ We've seen this before... impulse invariance

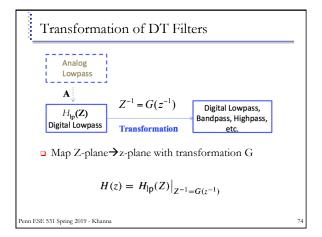
### Bilinear Transformation

 $\Box$  The technique uses an algebraic transformation between the variables s and z that maps the entire j  $\Omega$ -axis in the s-plane to one revolution of the unit circle in the z-plane.

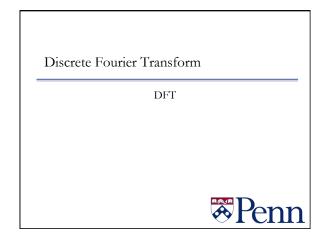
$$s = \frac{2}{T_d} \left( \frac{1 - z^{-1}}{1 + z^{-1}} \right);$$

$$H(z) = H_c \left( \frac{2}{T_d} \left( \frac{1 - z^{-1}}{1 + z^{-1}} \right) \right).$$

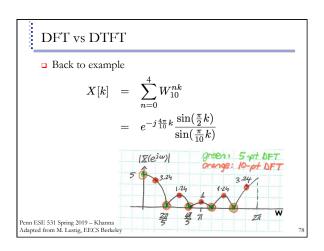
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# 



# Discrete Fourier Transform $x[n] = \frac{1}{N} \sum_{k=0}^{N-1} X[k] W_N^{-kn} \quad \text{Inverse DFT, synthesis}$ $X[k] = \sum_{n=0}^{N-1} x[n] W_N^{kn} \quad \text{DFT, analysis}$ It is understood that, $x[n] = 0 \quad \text{outside } 0 \leq n \leq N-1$ $X[k] = 0 \quad \text{outside } 0 \leq k \leq N-1$ Penn ESE 531 Spring 2019 – Khanna Adapted from M. Lastig, EECS Berkeley



# Circular Convolution • For $\mathbf{x}_1[n]$ and $\mathbf{x}_2[n]$ with length N $x_1[n] \ \textcircled{N} \ x_2[n] \leftrightarrow X_1[k] \cdot X_2[k]$ • Very useful!! (for linear convolutions with DFT)

## Linear Convolution via Circular Convolution

□ Zero-pad x[n] by P-1 zeros

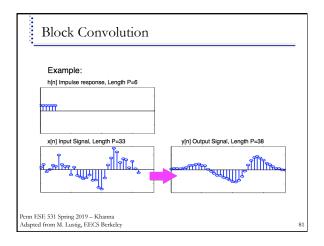
$$x_{\mathrm{zp}}[n] = \left\{ \begin{array}{ll} x[n] & 0 \leq n \leq L-1 \\ 0 & L \leq n \leq L+P-2 \end{array} \right.$$

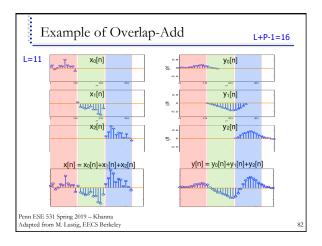
Zero-pad h[n] by L-1 zeros

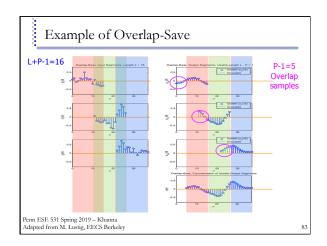
$$h_{\mathrm{zp}}[n] = \left\{ \begin{array}{ll} h[n] & 0 \leq n \leq P-1 \\ 0 & P \leq n \leq L+P-2 \end{array} \right.$$

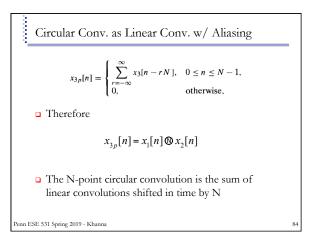
□ Now, both sequences are length M=L+P-1

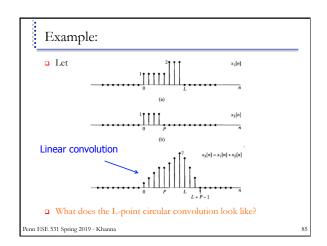
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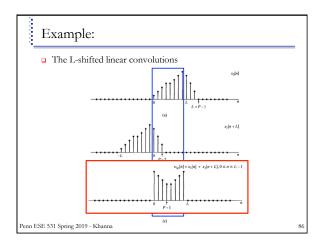


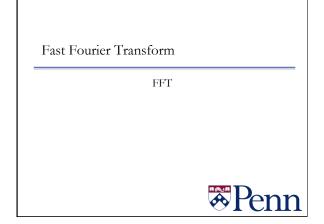


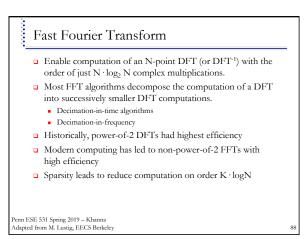


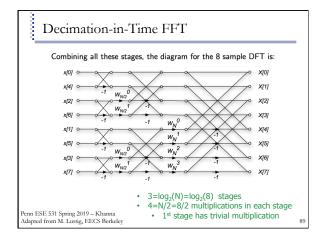


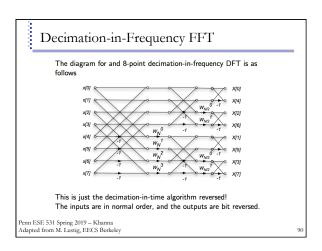






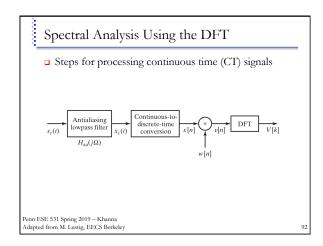






## Spectral Analysis





## Spectral Analysis Using the DFT

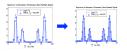
- □ Two important tools:
  - Applying a window → reduced artifacts
  - Zero-padding → increases spectral sampling

Parameter	Symbol	Units
Sampling interval	T	S
Sampling frequency	$\Omega_s = \frac{2\pi}{T}$	rad/s
Window length	L .	unitless
Window duration	$L \cdot T$	s
DFT length	$N \geq L$	unitless
DFT duration	N · T	s
Spectral resolution	$\frac{\Omega_s}{I} = \frac{2\pi}{I \cdot T}$	rad/s
Spectral sampling interval	$\frac{\Omega_s}{N} = \frac{2\pi}{N \cdot T}$	rad/s

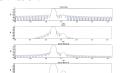
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# Frequency Analysis with DFT

- □ Length of window determines spectral resolution
- □ Type of window determines side-lobe amplitude/ main-lobe width
  - Some windows have better tradeoff between resolution and side-lobe height
- Zero-padding approximates the DTFT better. Does not introduce new information!



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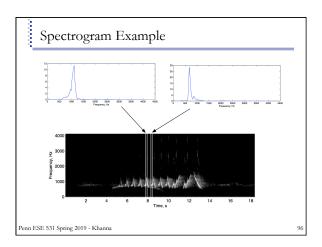


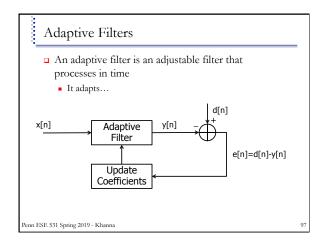
## Time Dependent Fourier Transform

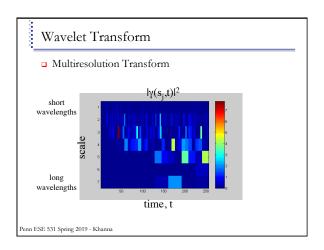
- □ Also called short-time Fourier transform
- □ To get temporal information, use part of the signal around every time point

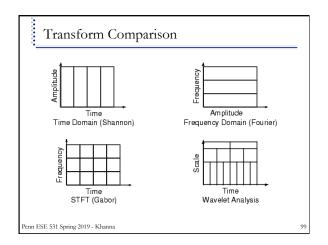
$$X[n,\lambda) = \sum_{m=-\infty}^{\infty} x[n+m]w[m]e^{-j\lambda m}$$

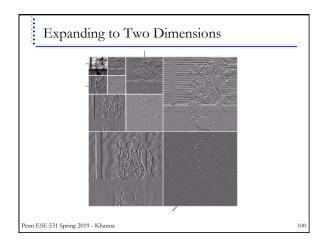
- □ Mapping from 1D  $\rightarrow$  2D, n discrete,  $\lambda$  cont.
- □ Simply slide a window and compute DTFT

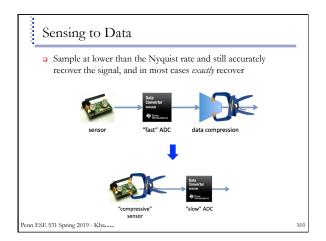


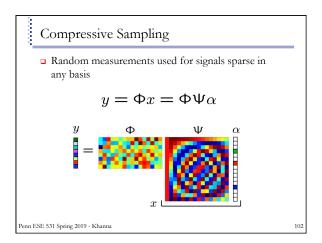












## Final Project

- □ Due today @midnight Project must be submitted into Canvas
  - No late projects accepted

Penn ESE 570 Spring 2019 - Khanna

### Admin

- □ Final Project due Apr 30<sup>th</sup>
  - No late accepted. Turn into Canvas on time.
- □ Last day of TA office hours Apr 30<sup>th</sup>
  - Piazza still available
- □ Last day of Tania office hours May 8<sup>th</sup>
- □ Final Exam Review Session May 10<sup>th</sup> (time TBD)
  - Watch Piazza for details
- □ Final Exam May 13<sup>th</sup>

## Final Exam Admin

- □ Final 5/13
  - Location Levine 101
  - Starts at exactly 3:00pm, ends at exactly 5:00pm (120 minutes)
  - Cumulative covers entire course
    - Except data converters, noise shaping (lec 12), adaptive filters (lec 23), wavelet transform (lec 25), and compressive sampling (lec 26)
  - Closed book
    - Data/Equation sheet provided by me
    - 2 8.5x11 two-sided cheat sheets allowed
    - Calculators allowed, no smart phones
  - Old exams posted
  - TA Review session on 5/10, Time and Place TBD
    - Watch Piazza for details