

ESE 5310: Digital Signal Processing

Lecture 16: March 28, 2024

FIR Filters (con't), Filter Transformations



Linear Filter Design

- ❑ Used to be an ambiguous process
 - Now, lots of tools to design optimal filters
- ❑ For DSP there are two common classes
 - Infinite impulse response IIR
 - Finite impulse response FIR
- ❑ Both classes use finite order of parameters for design
 - Filter order (ie. Length) restricts filter design



What is a Linear Filter?

- ❑ Attenuates certain frequencies
- ❑ Passes certain frequencies
- ❑ Affects both phase and magnitude

- ❑ IIR
 - Mostly non-linear phase response
 - Could be linear over a range of frequencies
- ❑ FIR
 - Much easier to control the phase
 - Both non-linear and linear phase

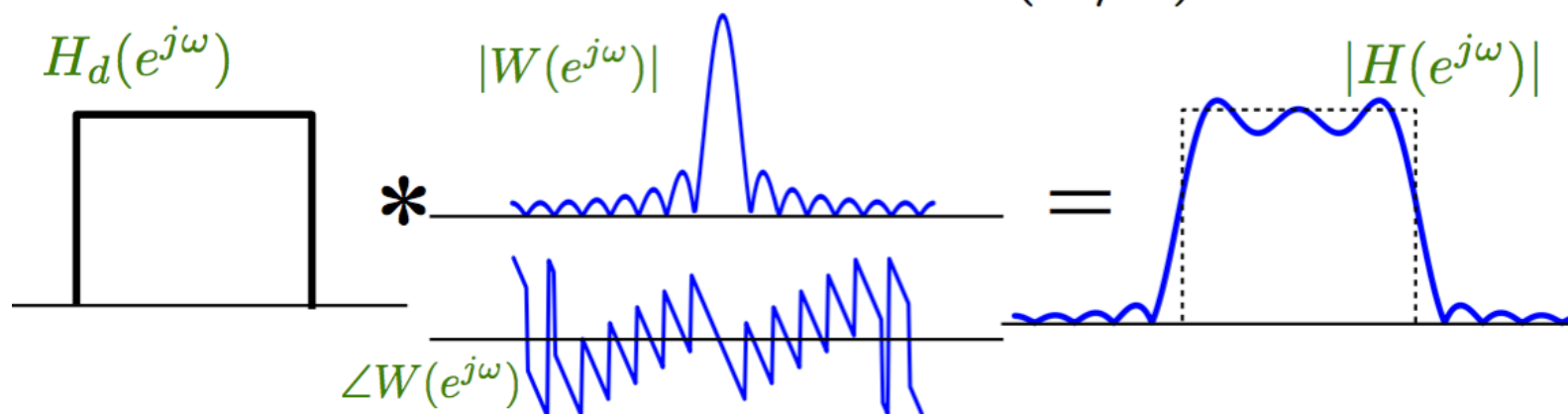
FIR Design by Windowing

- With multiplication in time property,

$$H(e^{j\omega}) = H_d(e^{j\omega}) * W(e^{j\omega})$$

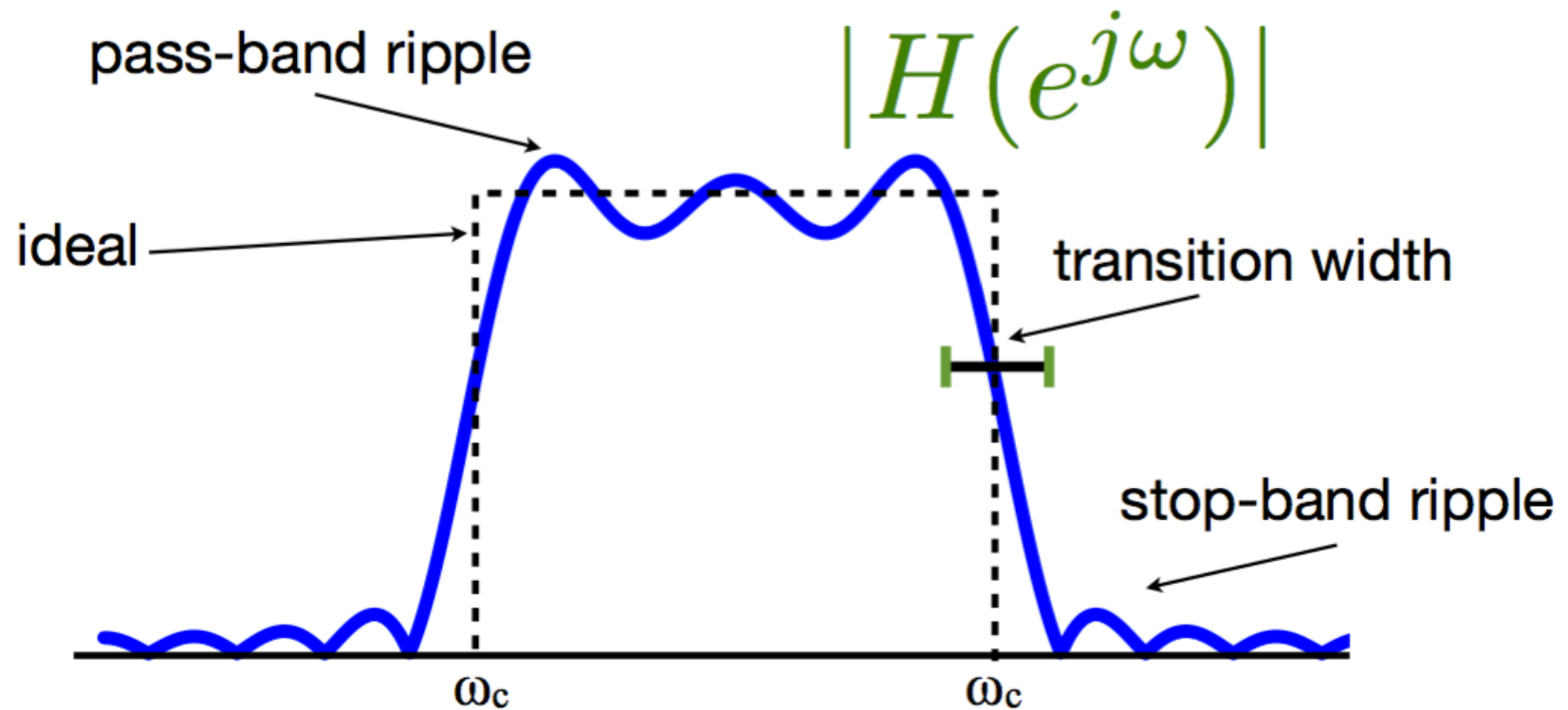
- For Boxcar (rectangular) window

$$W(e^{j\omega}) = e^{-j\omega \frac{M}{2}} \frac{\sin(\omega(M+1)/2)}{\sin(\omega/2)}$$





FIR Design by Windowing





Tapered Windows

Name(s)	Definition	MATLAB Command	Graph ($M = 8$)
Hann	$w[n] = \begin{cases} \frac{1}{2} \left[1 + \cos\left(\frac{\pi n}{M/2}\right) \right] & n \leq M/2 \\ 0 & n > M/2 \end{cases}$	<code>hann(M+1)</code>	
Hanning	$w[n] = \begin{cases} \frac{1}{2} \left[1 + \cos\left(\frac{\pi n}{M/2 + 1}\right) \right] & n \leq M/2 \\ 0 & n > M/2 \end{cases}$	<code>hanning(M+1)</code>	
Hamming	$w[n] = \begin{cases} 0.54 + 0.46 \cos\left(\frac{\pi n}{M/2}\right) & n \leq M/2 \\ 0 & n > M/2 \end{cases}$	<code>hamming(M+1)</code>	

Commonly Used Windows

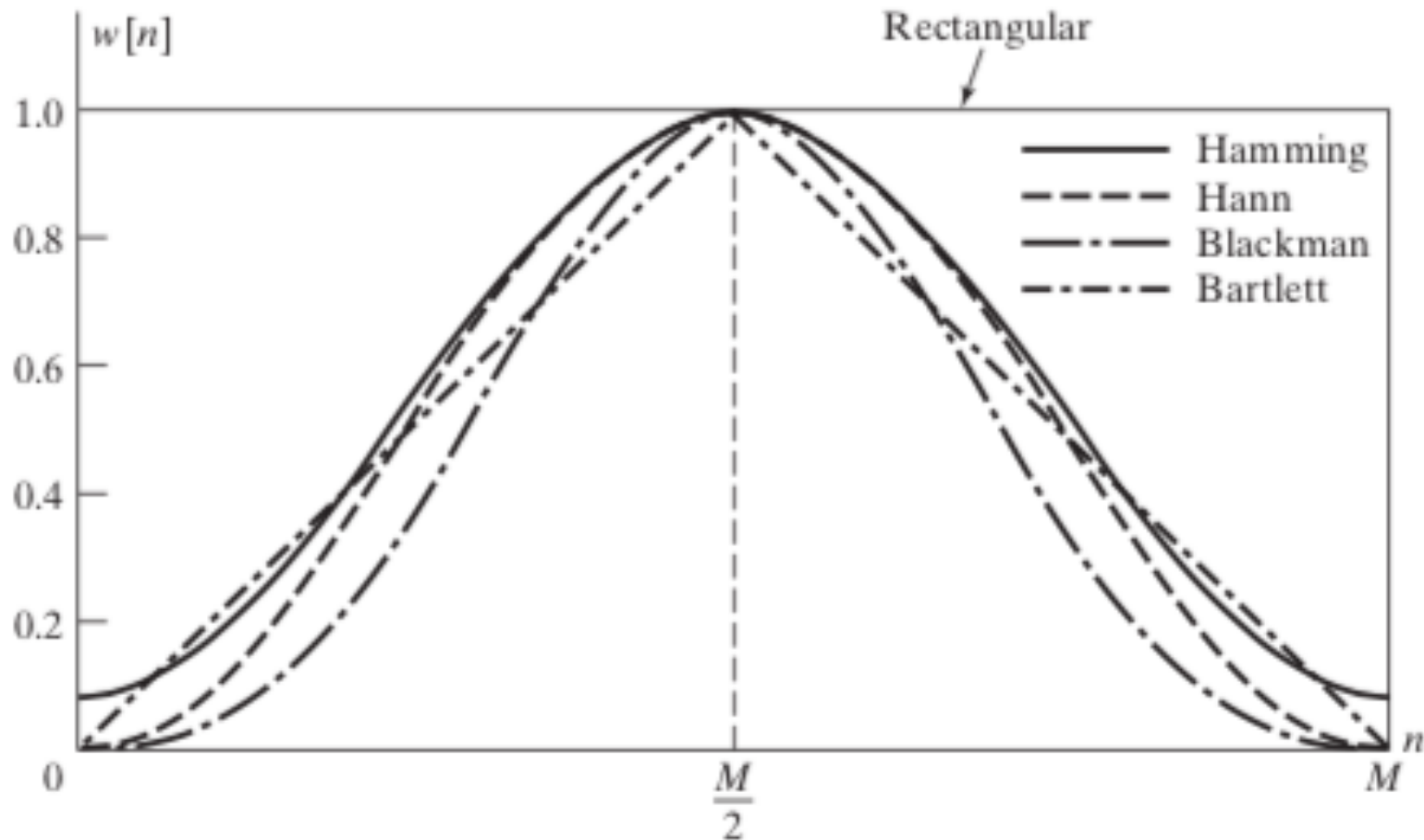


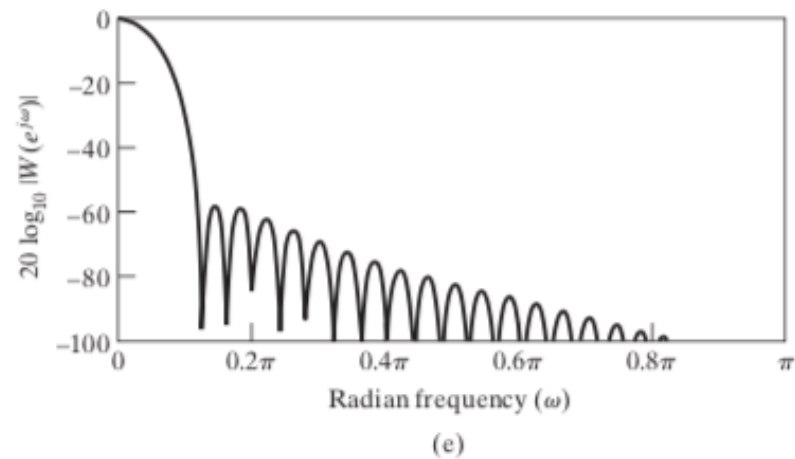
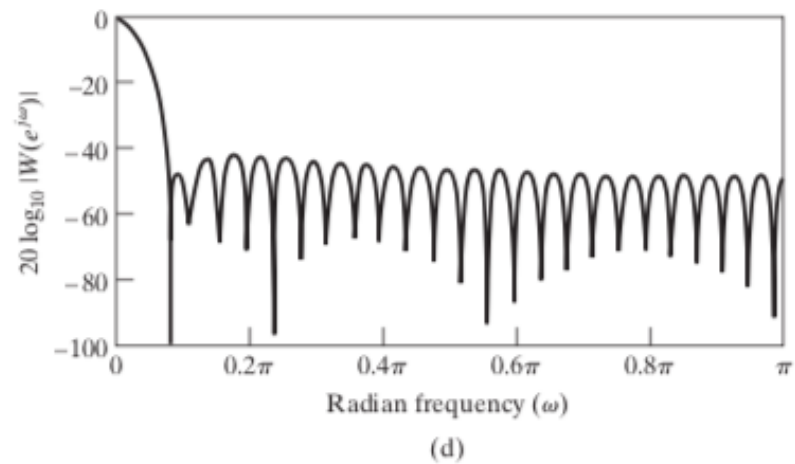
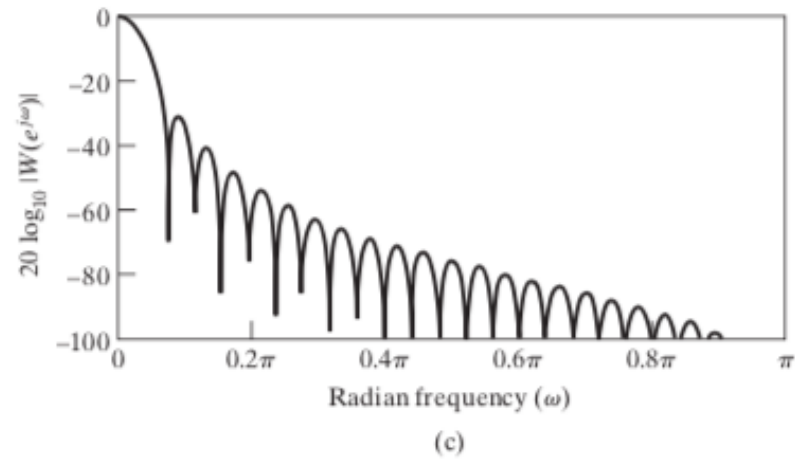
Figure 7.29 Commonly used windows.



Hann

Hamming

Blackman





Kaiser Window

- ❑ Near optimal window quantified as the window maximally concentrated around $\omega=0$

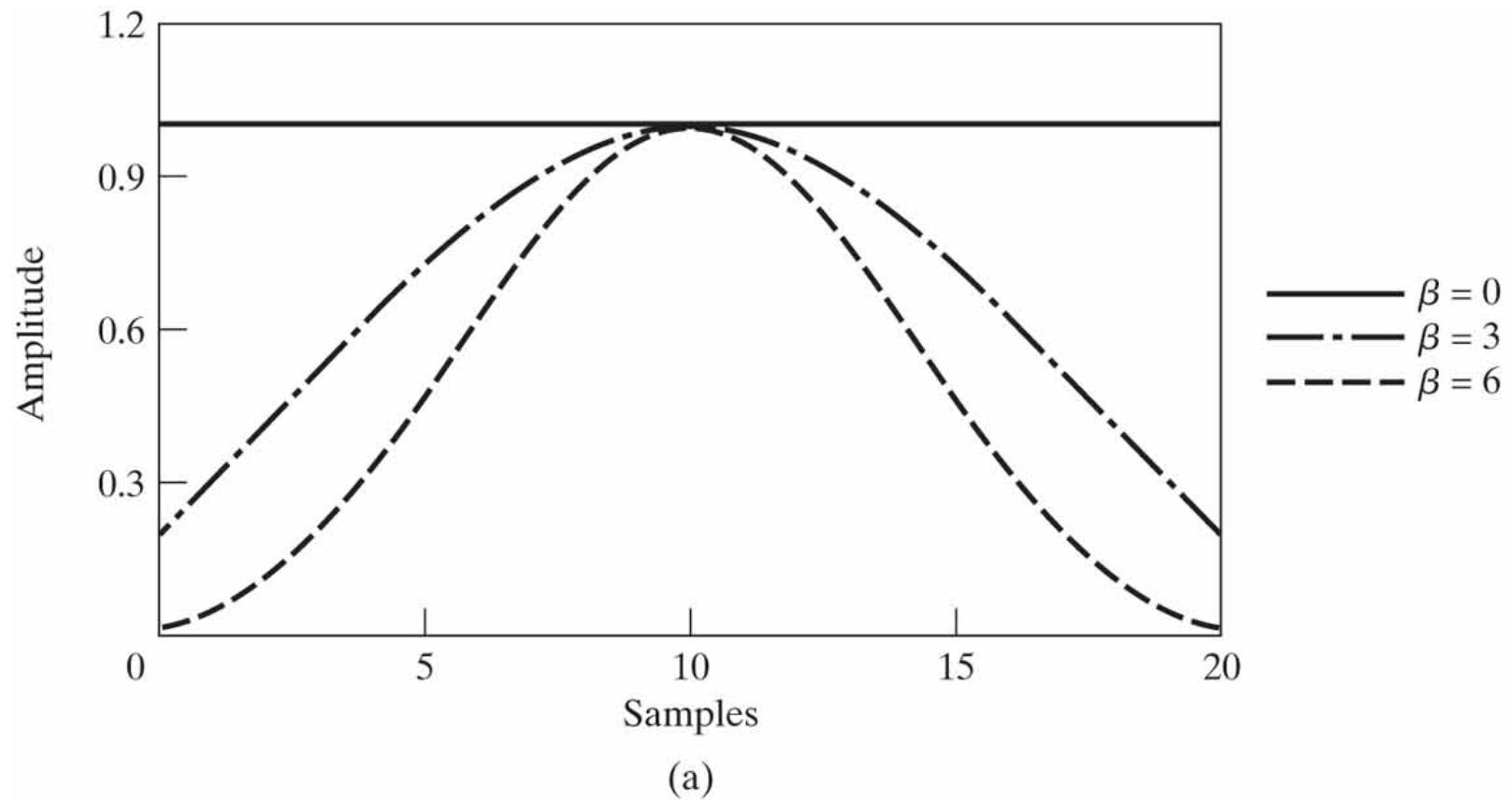
$$w[n] = \begin{cases} \frac{I_0[\beta(1 - [(n - \alpha)/\alpha]^2)^{1/2}]}{I_0(\beta)}, & 0 \leq n \leq M, \\ 0, & \text{otherwise,} \end{cases}$$

- ❑ Two parameters – M and β
- ❑ $\alpha=M/2$
- ❑ $I_0(x)$ – zeroth order Bessel function of the first kind



Kaiser Window

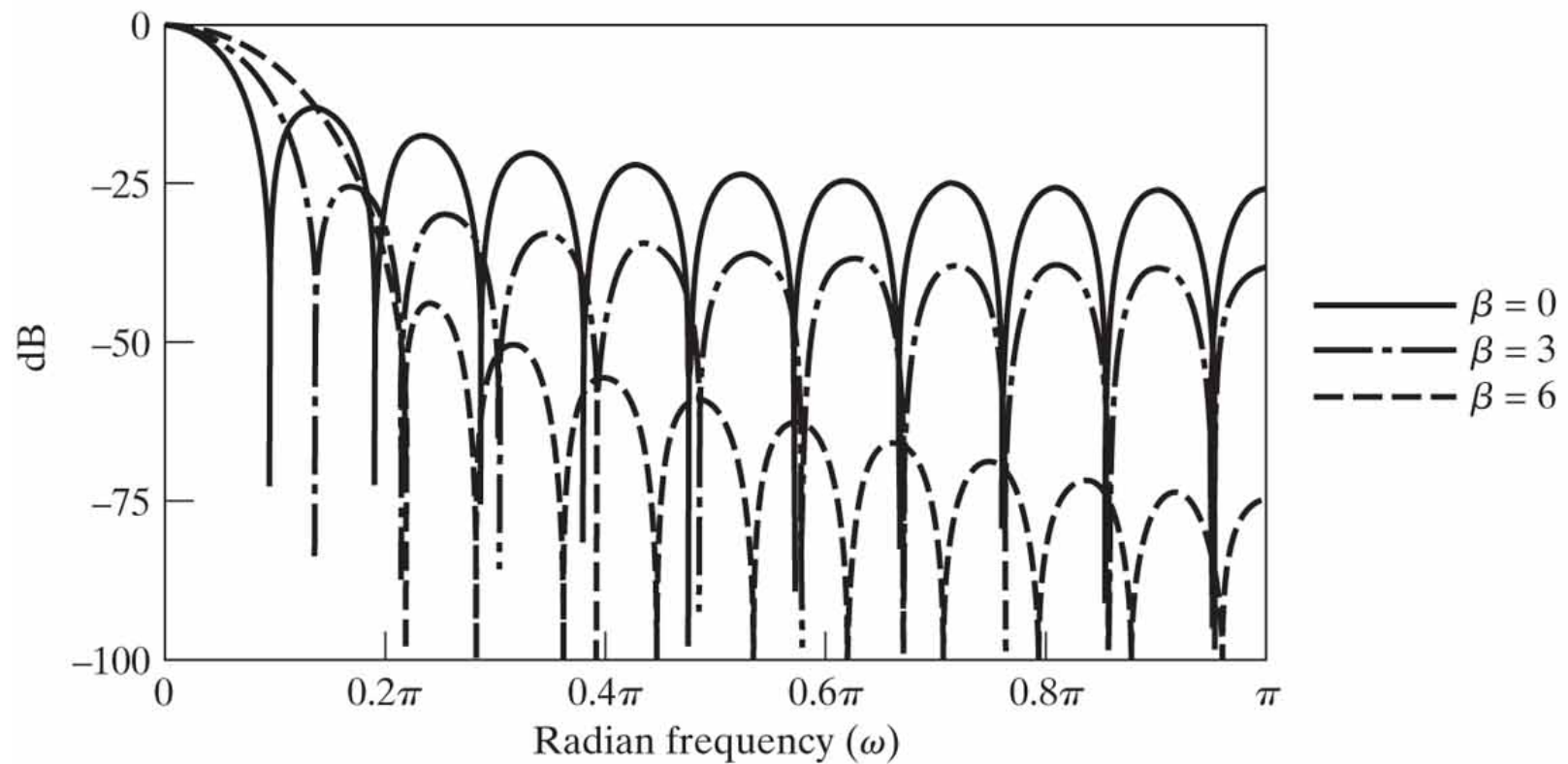
□ $M=20$





Kaiser Window

□ $M=20$

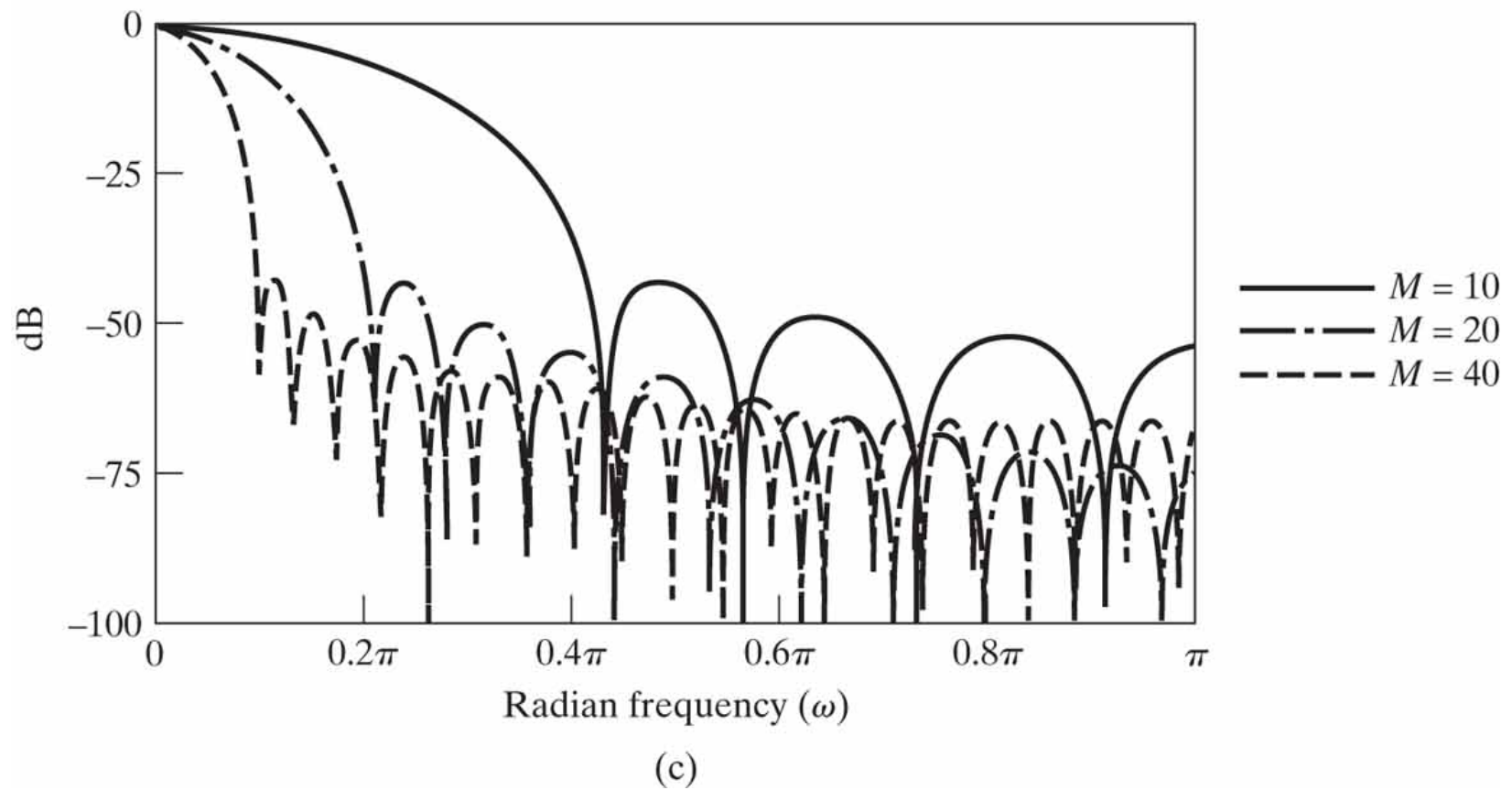


(b)



Kaiser Window

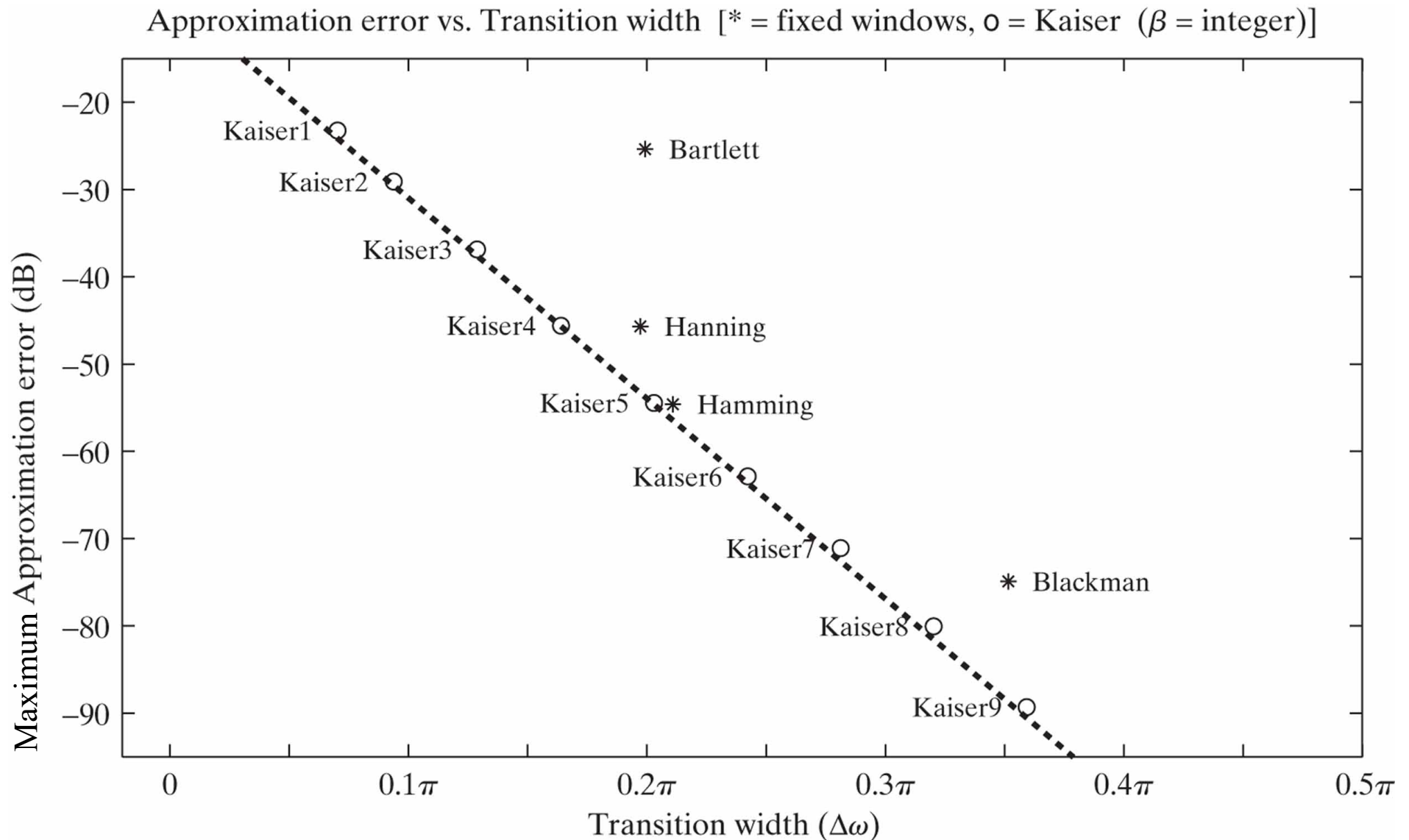
□ $\beta=6$





Approximation Error

LPF, $M=32$, $\omega_c=0.5\pi$





FIR Filter Design Process

- ❑ Choose a desired frequency response $H_d(e^{j\omega})$
 - non causal (zero-delay), and infinite imp. response
 - If derived from C.T, choose T and use:

$$H_d(e^{j\omega}) = H_c(j\frac{\Omega}{T})$$

- ❑ Window:
 - Length $M+1 \Leftrightarrow$ affects transition width
 - Type of window $\Leftrightarrow$ transition-width/ ripple

FIR Filter Design Process

- Choose a desired frequency response $H_d(e^{j\omega})$
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- Window:
 - Length $M+1 \Leftrightarrow$ affects transition width
 - Type of window $\Leftrightarrow$ transition-width/ ripple
 - Modulate to shift impulse response
 - Why?

$$H_d(e^{j\omega})e^{-j\omega\frac{M}{2}}$$



FIR Filter Design Process

- Determine truncated impulse response $h_1[n]$

$$h_1[n] = \begin{cases} \frac{1}{2\pi} \int_{-\pi}^{\pi} H_d(e^{j\omega}) e^{-j\omega \frac{M}{2}} e^{j\omega n} & 0 \leq n \leq M \\ 0 & \text{otherwise} \end{cases}$$

- Apply window

$$h_w[n] = w[n]h_1[n]$$

- Check:
 - Compute $H_w(e^{j\omega})$, if does not meet specs increase M or change window

Example: FIR Low-Pass Filter Design

$$H_d(e^{j\omega}) = \begin{cases} 1 & |\omega| \leq \omega_c \\ 0 & \text{otherwise} \end{cases}$$

Choose $M \Rightarrow$ Window length and set

$$H_1(e^{j\omega}) = H_d(e^{j\omega})e^{-j\omega \frac{M}{2}}$$

$$h_1[n] = \begin{cases} \frac{\sin(\omega_c(n-M/2))}{\pi(n-M/2)} & 0 \leq n \leq M \\ 0 & \text{otherwise} \end{cases}$$


$$\frac{\omega_c}{\pi} \text{sinc}\left(\frac{\omega_c}{\pi}(n - M/2)\right)$$

Example: FIR Low-Pass Filter Design

- The result is a windowed sinc function

$$h_w[n] = w[n]h_1[n]$$


$$\frac{\omega_c}{\pi} \text{sinc}\left(\frac{\omega_c}{\pi}(n - M/2)\right)$$

- High Pass Design:

- Design low pass
- Transform to $h_w[n](-1)^n$

- General bandpass

- Transform to $2h_w[n]\cos(\omega_0 n)$ or $2h_w[n]\sin(\omega_0 n)$



Design through FFT

- ❑ To design order M filter:
- ❑ Over-Sample/discretize the frequency response at P points where $P \gg M$ ($P=15M$ is good)

$$H_1(e^{j\omega_k}) = H_d(e^{j\omega_k})e^{-j\omega_k \frac{M}{2}}$$

- ❑ Sampled at: $\omega_k = k \frac{2\pi}{P} \quad |k = [0, \dots, P-1]$
- ❑ Compute $h_1[n] = \text{IDFT}_P(H_1[k])$
- ❑ Apply M+1 length window:

$$h_w[n] = w[n]h_1[n]$$



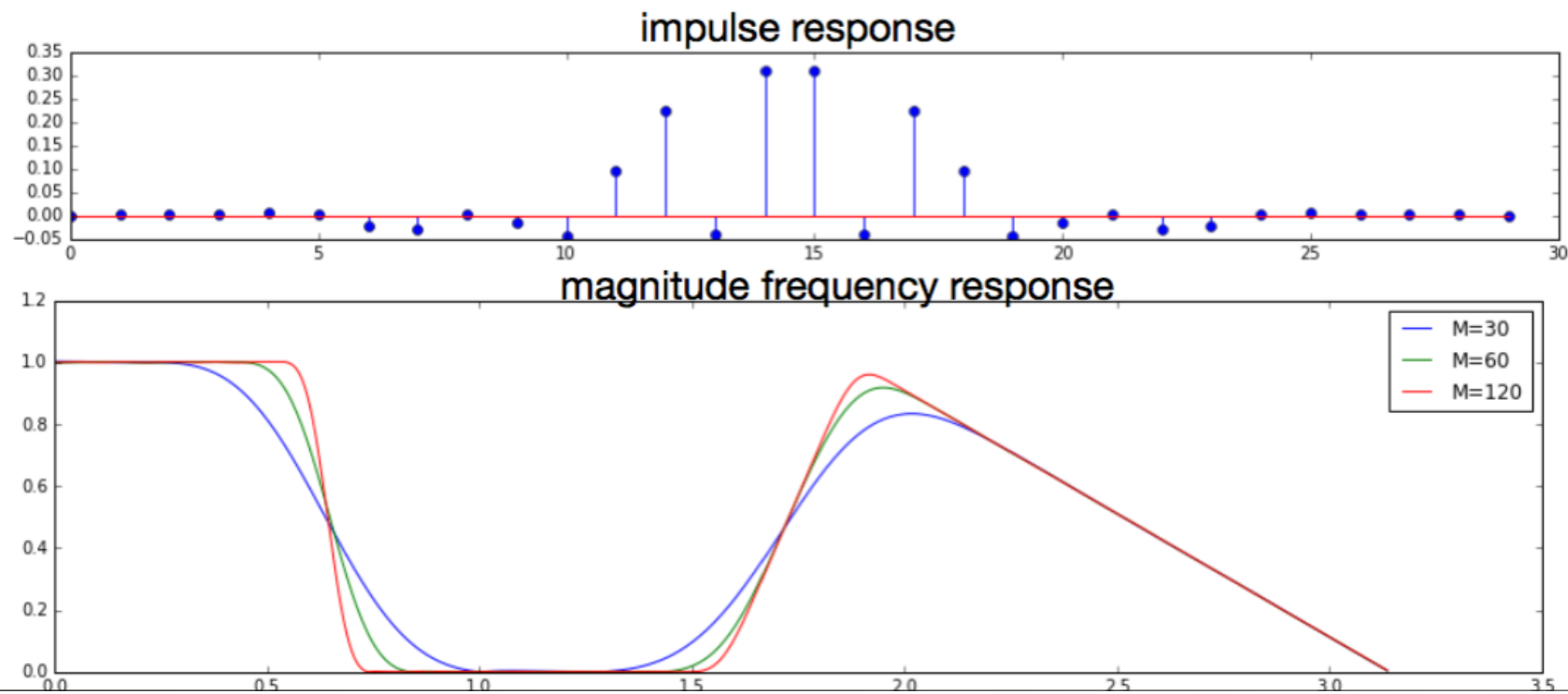
Example

- `signal.firwin2(M+1, omega_vec/pi, amp_vec)`
- `taps1 = signal.firwin2(30, [0.0, 0.2, 0.21, 0.5, 0.6, 1.0], [1.0, 1.0, 0.0, 0.0, 1.0, 0.0])`

`[0.0 0.2 0.21 0.5 0.6 1.0]`
`[1.0 1.0 0.0 0.0 1.0 0.0]`

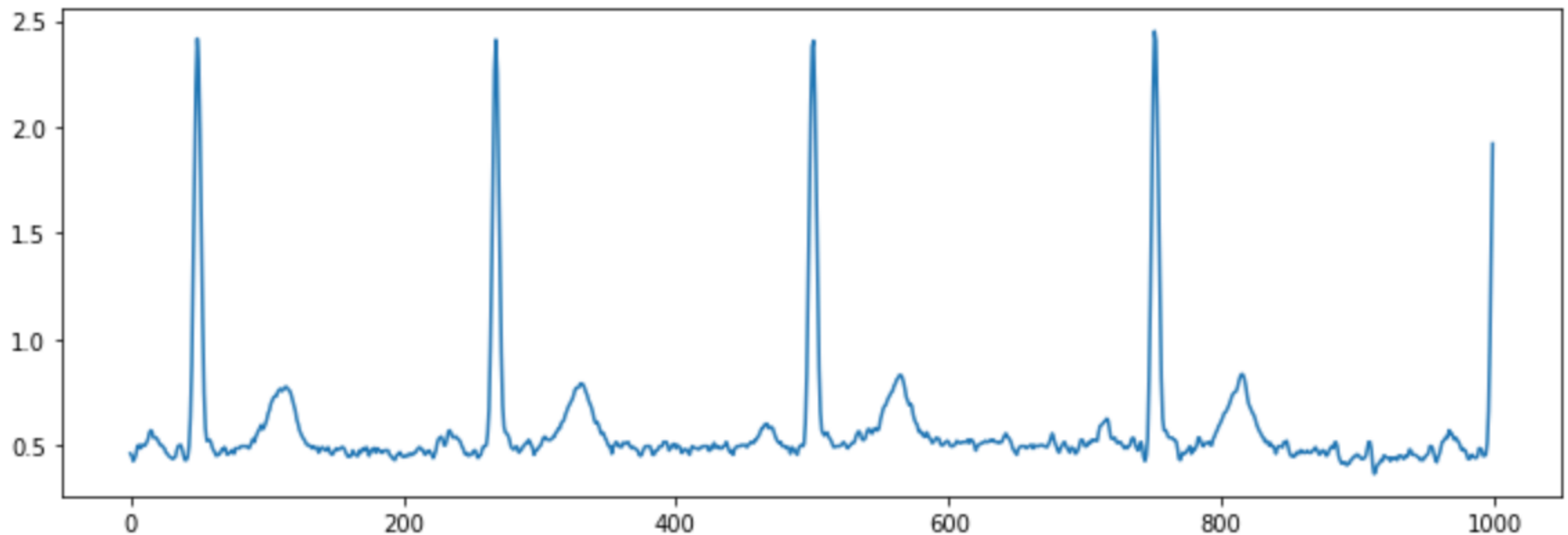
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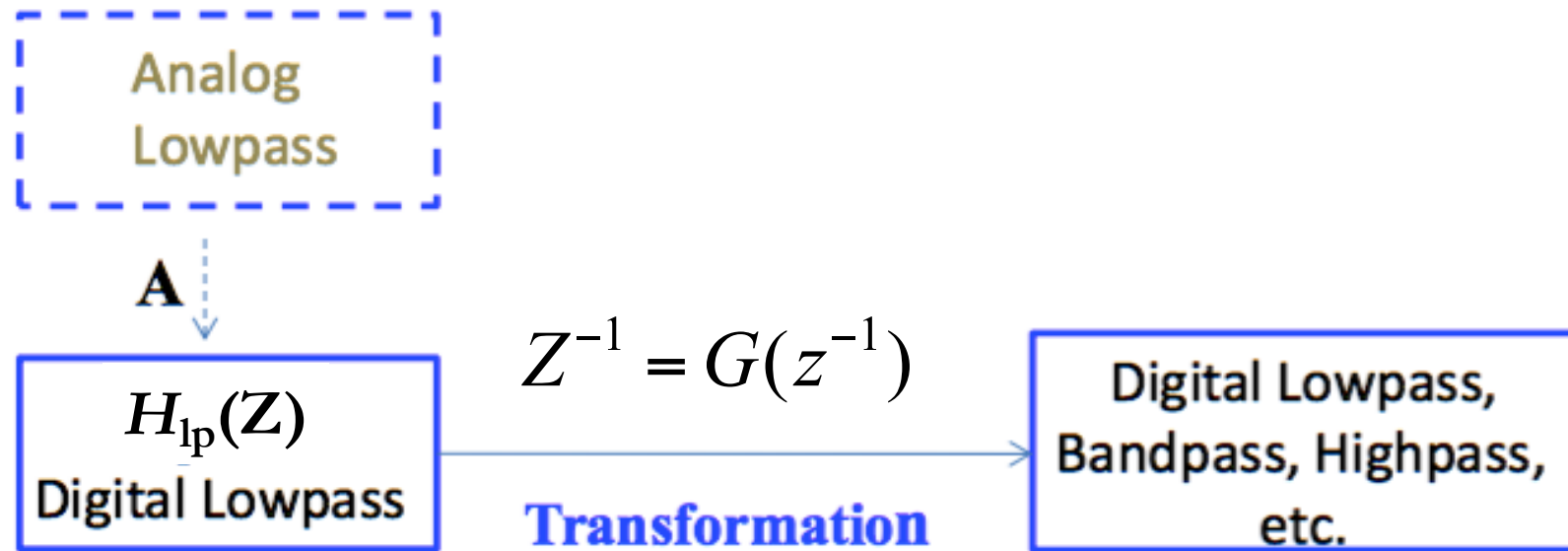


Python Filter/Re-sample Example

- ❑ Heartrate detection of ECG signal

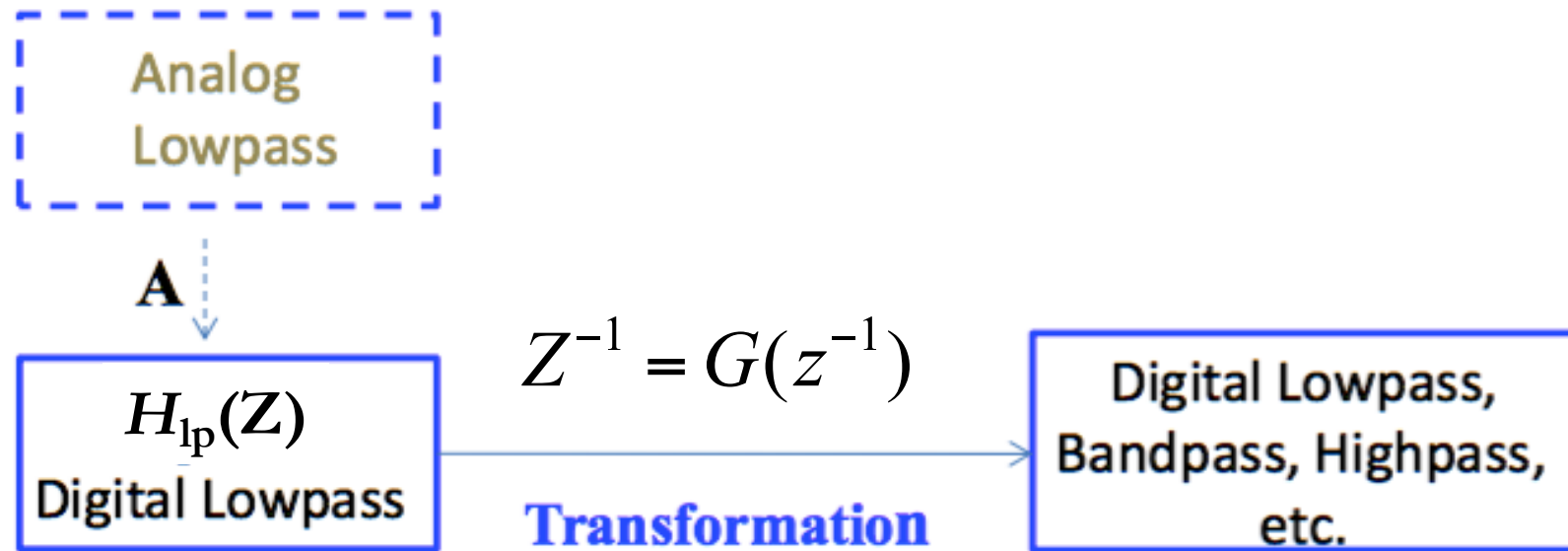


Transformation of DT Filters



- ❑ Z – complex variable for the LP filter
- ❑ z – complex variable for the transformed filter
- ❑ Map Z -plane $\rightarrow$ z -plane with transformation G

Transformation of DT Filters



- Map Z-plane $\rightarrow$ z-plane with transformation G

$$H(z) = H_{lp}(Z) \big|_{Z^{-1}=G(z^{-1})}$$



Example 1:

- Lowpass $\rightarrow$ highpass
 - Shift frequency by π

so $\omega \rightarrow \omega - \pi$ (Lowpass to highpass)



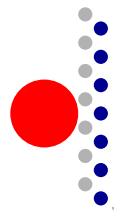
Example 1:

□ Lowpass $\rightarrow$ highpass

■ Shift frequency by π

so $\omega \rightarrow \omega - \pi$ (Lowpass to highpass)

$$G(z^{-1}) = -z^{-1} \quad \text{or} \quad e^{-j\omega} \rightarrow e^{-j(\omega - \pi)}$$



Example 1:

□ Lowpass $\rightarrow$ highpass

■ Shift frequency by π

$$G(z^{-1}) = -z^{-1}$$

ω	z	$ H_{lp}(z) = \left \frac{0.1}{1 - 0.9z^{-1}} \right $	$ H_{hp}(z) = \left \frac{0.1}{1 + 0.9z^{-1}} \right $
0			
$\frac{\pi}{2}$			
π			
$\frac{3\pi}{2}$			
2π			



Example 2:

□ Lowpass $\rightarrow$ bandpass

$$G(z^{-1}) = -z^{-2}$$



Example 2:

□ Lowpass $\rightarrow$ bandpass

$$G(z^{-1}) = -z^{-2}$$

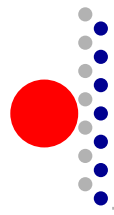
$$H_{lp}(z) = \frac{1}{1 - az^{-1}}$$

Pole at $z=a$

$\longrightarrow$

$$H_{bp}(z) = \frac{1}{1 + az^{-2}}$$

Pole at $z = \pm j\sqrt{a}$



Example 2:

□ Lowpass $\rightarrow$ bandpass

$$G(z^{-1}) = -z^{-2}$$

ω	z	$ H_{lp}(z) = \left \frac{0.1}{1 - 0.9z^{-1}} \right $	$ H_{bp}(z) = \left \frac{0.1}{1 + 0.9z^{-2}} \right $
0	1	1	
$\frac{\pi}{2}$	j	0.074	
π	-1	0.05	
$\frac{3\pi}{2}$	-j	0.074	
2π	1	1	



Example 3:

□ Lowpass $\rightarrow$ bandstop

$$Z^{-1} = G(z^{-1}) = z^{-2}$$



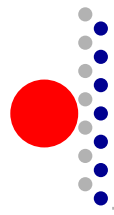
Example 3:

□ Lowpass $\rightarrow$ bandstop

$$Z^{-1} = G(z^{-1}) = z^{-2}$$

$$H_{lp}(z) = \frac{1}{1 - az^{-1}} \quad \longrightarrow \quad H_{bs}(z) = \frac{1}{1 - az^{-2}}$$

Pole at $z = \pm \sqrt{a}$



Example 2:

□ Lowpass $\rightarrow$ bandstop

$$G(z^{-1}) = z^{-2}$$

ω	z	$ H_{lp}(z) = \left \frac{0.1}{1 - 0.9z^{-1}} \right $	$ H_{bs}(z) = \left \frac{0.1}{1 - 0.9z^{-2}} \right $
0	1	1	
$\frac{\pi}{2}$	j	0.074	
π	-1	0.05	
$\frac{3\pi}{2}$	-j	0.074	
2π	1	1	



Transformation Constraints on $G(z^{-1})$

- If $H_{lp}(Z)$ is the rational system function of a causal and stable system, we naturally require that the transformed system function $H(z)$ be a rational function and that the system also be causal and stable.
 - $G(Z^{-1})$ must be a rational function of z^{-1}
 - The inside of the unit circle of the Z -plane must map to the inside of the unit circle of the z -plane
 - The unit circle of the Z -plane must map onto the unit circle of the z -plane.



Transformation Constraints on $G(z^{-1})$

- Respective unit circles in both planes

$$Z \triangleq e^{j\theta} \text{ and } z \triangleq e^{j\omega}$$



Transformation Constraints on $G(z^{-1})$

- Respective unit circles in both planes

$$Z = e^{j\theta} \text{ and } z = e^{j\omega}$$

$$Z^{-1} = G(z^{-1})$$

$$e^{-j\theta} = G(e^{-j\omega})$$

$$e^{-j\theta} = \left| G(e^{-j\omega}) \right| e^{j\angle G(e^{-j\omega})}$$

Transformation Constraints on $G(z^{-1})$

- Respective unit circles in both planes

$$Z = e^{j\theta} \text{ and } z = e^{j\omega}$$

$$Z^{-1} = G(z^{-1})$$

$$e^{-j\theta} = G(e^{-j\omega})$$

$$e^{-j\theta} = |G(e^{-j\omega})| e^{j\angle G(e^{-j\omega})}$$

$$1 = |G(e^{-j\omega})| \quad -\theta = \angle G(e^{-j\omega})$$



Transformation Constraints on $G(z^{-1})$

□ General form that meets all constraints:

- a_k real and $|a_k| < 1$

$$G(z^{-1}) = \pm \prod_{k=1}^N \frac{z^{-1} - \alpha_k}{1 - \alpha_k z^{-1}}$$



General Transformation

- ❑ Lowpass $\rightarrow$ lowpass

$$G(z^{-1}) = \frac{z^{-1} - \alpha}{1 - \alpha z^{-1}}$$

- ❑ Changes passband/stopband edge frequencies

General Transformation

- Lowpass $\rightarrow$ lowpass

$$G(z^{-1}) = \frac{z^{-1} - \alpha}{1 - \alpha z^{-1}}$$

- Changes passband/stopband edge frequencies

From $e^{-j\theta} = \frac{e^{-j\omega} - \alpha}{1 - \alpha e^{-j\omega}}$, get

$$\omega(\theta) = \tan^{-1} \left(\frac{(1 - \alpha^2) \sin(\theta)}{2\alpha + (1 + \alpha^2) \cos(\theta)} \right)$$

General Transformation

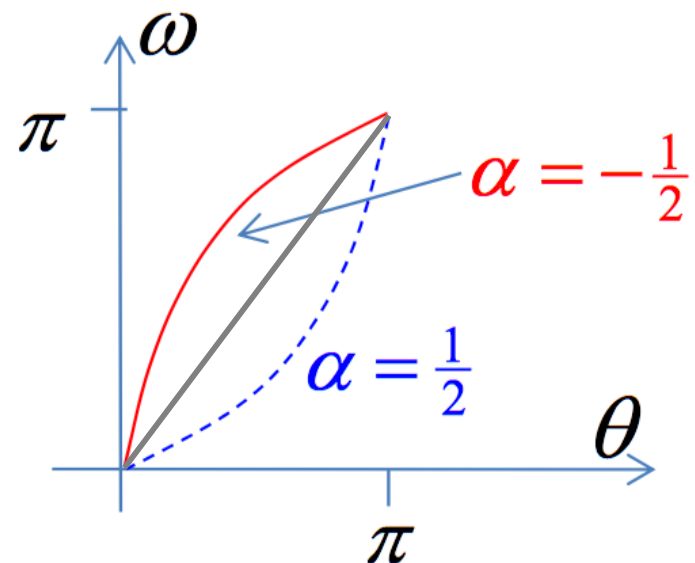
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$$\omega(\theta) = \tan^{-1} \left(\frac{(1 - \alpha^2) \sin(\theta)}{2\alpha + (1 + \alpha^2) \cos(\theta)} \right)$$





General Transformations

TABLE 7.1 TRANSFORMATIONS FROM A LOWPASS DIGITAL FILTER PROTOTYPE OF CUTOFF FREQUENCY θ_p TO HIGHPASS, BANDPASS, AND BANDSTOP FILTERS

Filter Type	Transformations	Associated Design Formulas
Lowpass	$Z^{-1} = \frac{z^{-1} - \alpha}{1 - \alpha z^{-1}}$	$\alpha = \frac{\sin\left(\frac{\theta_p - \omega_p}{2}\right)}{\sin\left(\frac{\theta_p + \omega_p}{2}\right)}$ $\omega_p = \text{desired cutoff frequency}$
Highpass	$Z^{-1} = -\frac{z^{-1} + \alpha}{1 + \alpha z^{-1}}$	$\alpha = -\frac{\cos\left(\frac{\theta_p + \omega_p}{2}\right)}{\cos\left(\frac{\theta_p - \omega_p}{2}\right)}$ $\omega_p = \text{desired cutoff frequency}$
Bandpass	$Z^{-1} = -\frac{z^{-2} - \frac{2\alpha k}{k+1}z^{-1} + \frac{k-1}{k+1}}{\frac{k-1}{k+1}z^{-2} - \frac{2\alpha k}{k+1}z^{-1} + 1}$	$\alpha = \frac{\cos\left(\frac{\omega_{p2} + \omega_{p1}}{2}\right)}{\cos\left(\frac{\omega_{p2} - \omega_{p1}}{2}\right)}$ $k = \cot\left(\frac{\omega_{p2} - \omega_{p1}}{2}\right) \tan\left(\frac{\theta_p}{2}\right)$ $\omega_{p1} = \text{desired lower cutoff frequency}$ $\omega_{p2} = \text{desired upper cutoff frequency}$
Bandstop	$Z^{-1} = \frac{z^{-2} - \frac{2\alpha}{1+k}z^{-1} + \frac{1-k}{1+k}}{\frac{1-k}{1+k}z^{-2} - \frac{2\alpha}{1+k}z^{-1} + 1}$	$\alpha = \frac{\cos\left(\frac{\omega_{p2} + \omega_{p1}}{2}\right)}{\cos\left(\frac{\omega_{p2} - \omega_{p1}}{2}\right)}$ $k = \tan\left(\frac{\omega_{p2} - \omega_{p1}}{2}\right) \tan\left(\frac{\theta_p}{2}\right)$ $\omega_{p1} = \text{desired lower cutoff frequency}$ $\omega_{p2} = \text{desired upper cutoff frequency}$



Big Idea

□ FIR

- Use desired frequency response to generate desired impulse responses
- Use filter order and window type to meet specs

□ DT filter transformations

- Transform z -plane with rational function $G(z^{-1})$
 - Constraints on G for causal/stable systems



Admin

- ❑ Proj 1 due Tuesday 4/2